NATIONAL ADVISORY COMMITTEE FOR AERONAUTICS

WARTIME REPORT

ORIGINALLY ISSUED

January 1943 as Advance Restricted Report

FLIGHT INVESTIGATION OF NACA DS COWLINGS ON THE XP-42 AIRPLANE

III - LOW-INLET-VELOCITY COWLING WITHOUT FAN OR PROPELLER

CUFFS, WITH AXIAL-FLOW FAN ALONE, AND WITH TWO

DIFFERENT SETS OF PROPELLER CUFFS

By J. Ford Johnston and T. J. Voglewede

Langley Memorial Aeronautical Laboratory
Langley Field, Va.

To be returned to the files of the National Advisory Committee for Aeronautics Shington D. C.



WASHINGTON

NACA WARTIME REPORTS are reprints of papers originally issued to provide rapid distribution of advance research results to an authorized group requiring them for the war effort. They were previously held under a security status but are now unclassified. Some of these reports were not technically edited. All have been reproduced without change in order to expedite general distribution.

ADVANCE RESTRICTED REPORT

FLIGHT INVESTIGATION OF NACA DS COWLINGS ON THE XP-42 AIRPLANE

III - LOW-INLET-VELOCITY COWLING WITHOUT FAN OR PROPELLER

CUFFS. WITH AXIAL-FLOW FAN ALONE, AND WITH TWO

DIFFERENT SETS OF PROPELLER CUFFS

By J. Ford Johnston and T. J. Voglewede

SUMMARY

The results of flight measurements of the performance and cooling characteristics of the XP-42 airplane equipped with a short-nose low-inlet-velocity cowling are given. The tests include measurements in high-speed level flight and in climb of the effects of: (1) a spinner-mounted axial-flow fan without propeller cuffs; (2) no fan or cuffs; and (3) two different sets of propeller cuffs. This cowling is one of a series being tested in an effort to improve the characteristics of radial air-cooled engine installations.

The maximum speed of the airplane without fan or cuffs, when corrected to military power (1000 hp at 14,500 ft), was 343 miles per hour; with No. 2 cuff set, 342 miles per hour; with No. 1 cuff set or with the fan, 339 miles per hour.

The cooling-air-pressure recovery on the front of the engine in the high-speed level-flight condition averaged 76 percent of free-stream impact pressure without fan or cuffs, 77 percent with cuffs 2, 80 percent with cuffs 1, and 84 percent with the axial-flow fan. In full-power climb at 140 miles per hour at 14,000 feet, the pressure recoveries were 74, 84, 84, and 97 percent of free-stream impact pressure in this same order.

Ground-cooling tests showed that engine cylinder and accessory temperatures were appreciably higher without fan or cuffs. Oil-in and rear-spark-plug-elbow temperatures exceeded their limits in this condition when corrected to Army standards.

INTRODUCTION

The NACA is conducting an extensive series of flight tests of several types of cowling, as outlined in references 1 and 2, in an attempt to improve the characteristics of radial air-cooled engine installations. The conditions so far investigated include:

Test	Airplane and flight condition
1	Long-nose high-inlet-velocity cowling with small cowl flaps; high speed
2	Long-nose high-inlet-velocity cowling with modified cowl flaps; climb
3	Short-nose high-inlet-velocity cowling with small cowl flaps; high speed
4	Short-nose low-inlet-velocity cowling with spinner-mounted axial-flow fan, cuffs 1, and small cowl flaps; high speed
5	Short-nose low-inlet-velocity cowling with fan, cuffs 1, and modified cowl flaps; climb
6	Short-nose low-inlet-velocity cowling with fan, cuffs 1, and modified cowl flaps; high speed
7	Short-nose low-inlet-velocity cowling with fan, cuffs 1, and modified cowl flaps; baffle seal strips at base of cylinders removed; high speed
8	Short-nose low-inlet-velocity cowling with fan only; high speed
9	Short-nose low-inlet-velocity cowling with fan only; climb
10	Short-nose low-inlet-velocity cowling with- out fan or cuffs; climb
11	Short-nose low-inlet-velocity cowling with- out fan or cuffs; high speed

12		low-inlet-velocity cowling with without fan; high speed
13		low-inlet-velocity cowling with without fan; climb
14		low-inlet-velocity cowling with without fan; climb
15		low-inlet-velocity cowling with without fan: high speed

The results of tests 1 and 2 are described in reference 1, of test 3 in reference 2, and of tests 4 to 7 in reference 3. The present paper gives the results of tests 8 to 15, which represent high-speed and climb tests of variations of the fan and cuff arrangement on the cowling described in reference 3.

The design of the cowling and engine installation was a project of the Air-Cooled Engine-Installation Group stationed at the Laboratory. The members of the group associated with this project included Mr. Howard S. Ditsch of the Curtiss-Wright Corporation, Mr. Peter Torraco of the Republic Aviation Corporation, Mr. William S. Richards of the Wright Aeronautical Corporation, and Mr. James R. Thompson of Pratt & Whitney Aircraft. The Materiel Command, Army Air Forces, sponsored the investigation and supplied the XP-42 airplane. The Curtiss-Wright Corporation, Airplane Division, handled the construction as well as the structural and detail design of the cowling and supplied personnel to assist in the servicing and maintenance of the airplane and cowling during the tests. Pratt & Whitney Aircraft prepared the engine and torque meter for the tests and assisted in the operation and servicing of the engine. The propeller, cuffs, and spin-ner were supplied by the Curtiss-Wright Corporation, Propeller Division.

XP-42 AIRPLANE WITH SHORT-NOSE LOW-INLET-VELOCITY COWLING

The XP-42 airplane used in the tests is described in references 1 and 2. The installation of the short-nose low-inlet-velocity cowling and fan is described in reference 3. Figure 1 is a dimensioned drawing of the cowling showing both the fan and the cuffs in place, Figure 2 is

a side view of the airplane with cuff 1 and with modified cowl flaps. Figure 3 shows a close-up of the cowling after the fan blades had been machined off and with cuff 2 in place. The small adjustable cowl flaps originally provided are shown in the open position. The extra flaps for cooling in climb, which are adjustable on the ground only, are shown in the closed position.

As originally planned, there was to be a difference of 5° at the spinner between the pitch of the two sets of cuffs, all other characteristics being the same. After cuff 2 was fitted, measurements showed the average pitch angle of cuff 2 to be approximately $1\frac{1}{2}$ ° higher than that of cuff 1. The cuff sections at the 14-inch radius are shown in figure 4. Figure 5 compares the average section of each set by superposing the straight portion of their mean line. Although individual cuffs of either set varied only slightly in shape from the average for the set, it was found that individual cuff angles of the cuff 2 set varied from 30.8° to 33.5°. Cuff angles of the cuff 1 set varied only ± 0.1 ° from the average.

The airplane as prepared for the tests weighed about 6000 pounds with a 175-pound pilot and full tanks. It retained the standard aerial but had no provision for guns.

TEST APPARATUS AND PROCEDURE

The installation of the test equipment was described in reference 2.

Speed and cooling characteristics in level flight with military power were determined by making level runs at full throttle at 2700 rpm at and above the engine critical altitude, as described in reference 2. Two flights of five runs each were made for each high-speed test condition. The range of altitudes investigated was from 14,000 to 20,000 feet.

For climb tests with all cowling arrangements, two conditions have been investigated: (1) climb, at 155 miles per hour indicated airspeed in automatic rich, with manifold pressure limited to 40 inches of mercury and (2) climb at 140 miles per hour indicated airspeed in full rich, with manifold pressure limited to $43\frac{1}{2}$ inches of

mercury to 7000 feet, then $42\frac{1}{2}$ inches to full throttle. For tests 13 and 14, a third condition was investigated: climb at an indicated airspeed of 140 miles per hour with carburetor setting in automatic rich, with the manifold pressure limited to 40 inches of mercury.

On two occasions (with fan only and with cuffs 2) during the 140-mile-per-hour climbs with the manifold pressures previously specified for full-rich operation, the mixture control was inadvertently left in automatic rich for the first part of the climb, then changed to full rich.

All data were recorded automatically and continuously during the climbs. Under these conditions, a "run" was taken as the period of time for one cycle of the pressure switch or of the thermocouple switch,

The tests were made in the following sequence:

- (1) Test 9 (climb, fan only)
- (2) Test 8 (high speed, fan only)
- (3) Test 10 (climb, no fan or cuffs)
- (4) Test 11 (high speed, no fan or cuffs)
- (5) Test 15 (high speed, cuffs 2)
- (6) Test 12 (high speed, cuffs 1)
- (7) Test 13 (climb, cuffs 1)
- (8) Test 14 (climb, cuffs 2)

The airplane and engine were given a 50-hour check between tests 11 and 15. During the check, the spark plugs were changed and valve clearances reset.

Ground-cooling tests were made for three of the four installations: without fan or cuffs, with cuffs 1, and with cuffs 2. The tests were made by running 10 minutes at 1380 rpm, 5 minutes idling, and 10 minutes with the engine cut off. Temperatures were recorded continuously during the tests.

Measurements of the propeller-cuff sections were obtained by photographic means. A rubber strip 1/2 inch thick was laid around the cuff in a plane perpendicular to the blade axis and approximately 14 inches from the axis of rotation of the propeller. A thin flat steel bar was laid on the propeller-blade chord at the 42-inch radius. Photographs were then taken with the blade axis pointing directly into the telescopic camera, which was placed approximately 40 feet from the cuff. The result was an outline of the cuff section with the chord line at the 42-inch radius superposed upon it as a reference.

SYMBOLS

- o density ratio
- n propulsive efficiency
- S wing area
- q impact pressure
- Q volume flow of free air, cubic feet per minute
- Δp average pressure drop across engine, inches of water
- On drag coefficient
- p observed pressure above free-stream static pressure, inches of water

RESULTS AND DISCUSSION

The data obtained in the high-speed and climb tests are given in tables I(a), I(b), and II. The main climb-test data are shown in figures 6 to 9 in the form of time histories of the climbs.

Maximum Speed

The values of maximum speed and power obtained during tests 8, 11, 12, and 15 are plotted against density altitude in figure 10. Inasmuch as the speed figures are

not directly comparable because of differences in power, they have been reduced in figure 11 to the parameters

$$\left(\frac{bhp}{\sigma}\right)^{1/3}$$
, representative of the effective power, and

$$52.73 \left(\frac{\eta}{SC_D}\right)^{1/3}$$
 representative of the aerodynamic refine-

ment. The product of these parameters is the airplane speed. It is evident that the installation having the highest value of the parameter $52.73 \left(\frac{\eta}{SC_D}\right)^{1/3}$ will have

the highest speed at a given power and altitude.

Measurements described in reference 3 showed that the addition of the fixed cowl flaps in the closed position reduced the top speed by two-thirds of 1 percent, or 2 miles per hour, from that obtained with the original cowl flaps. Because the drag of the modified cowl flaps is considered to be excessive in comparison with the drag of the best modern cowl-flap designs, the speeds obtained with the modified cowl flaps should be corrected to the original cowl-flap condition by adding approximately 2 miles per hour when comparisons with other installations are made. This correction has been incorporated in the data plotted in figure 12, which presents a comparison of the speeds obtained with the various cowling arrangements tested on the XP-42 airplane. Points obtained by the Army for similar airplanes with conventional air-cooled (P-36A) and liquid-cooled (P-4QC) installations are also shown.

Examination of figure 12 shows that, if in each case the engine had delivered its rated military power (1000 hp at 14,500 ft; $\frac{bhp}{\sigma}$ = 1564), the speeds obtained would

have been as follows:

Airplane condition	Maximum speed at 1000 hp at 14,500 ft (mph)
Long nose with cuffs	344
Short-nose high-inlet velocity with cuffs Short-nose low-inlet-velocity:	339
With fan and cuffs 1	337
Fan only	339
Cuffs 1, no fan	339
Cuffs 2, no fan	342
No fan or cuffs	343

The comparison shows that the use of fans or propeller cuffs for increasing available cooling pressures resulted in a slight decrease in speed.

The difference in maximum speed obtained with cuffs l and with cuffs 2 is larger than would be expected from the small differences between the cuffs, although this result is, to some extent, supported by the difference in cooling-air pressures on the front of the engine.

Pressures and Temperatures

The average cooling-air pressures on the engine are listed in table III for both the climb and the high-speed conditions. The pressures on the front of the engine in the high-speed level-flight condition averaged 0.84q_c with fan, 0.80q_c with cuffs 1, 0.77q_c with cuffs 2, and 0.76q_c without fan or cuffs. The distribution of these pressures around the engine for typical locations on the cylinders is shown in figure 13. The values plotted are the average values obtained during 10 runs for each location of pressure measurement. The plotted points show that the fan and cuffs had only minor effects on the pattern of pressure distribution although they raised the general pressure level.

The fact that the rear pressures varied between installations so as to maintain almost a constant pressure drop across the engine regardless of the front pressures was largely accidental, as it was difficult to return the cowl flaps to the same setting each time. When the cowlflap setting remained unchanged between tests with cuffs 2 and with cuffs 1, the rise in rear pressures was

approximately one-half the rise in front pressures, which was about the variation to be expected from the relative conductivities of engine and skirt exit.

Figure 14 shows the distribution of cooling-air pressures for a 140-mile-per-hour climb plotted as in figure 13. The points for each installation were taken from runs at approximately the same altitude, 13,000 to 14,000 feet. Because they are not averaged over a series of runs, the individual values may be subject to errors of approximately ±4 percent. Figure 14 shows that, in climb as in the high-speed condition, the fan and cuffs had no important effect on the pattern of pressure distribution around the engine. For the condition of the airplane without fan or cuffs, the front pressures averaged 0.74q; with either cuffs 1 or cuffs 2, 0.84q; and with the fan, 0.97q. These values are quoted for 140mile-per-hour climbs for carburetor settings in full rich at 13,000 to 14,000 feet; the same values were observed with cuffs 1 and cuffs 2 at 140 miles per hour in automatic rich. In the climbs at 155-miles per hour indicated airspeed in automatic rich at the same altitude, the values were 0.75qc without fan or cuffs, 0.82qc with either cuffs 1 or cuffs 2, and 0.95q with the fan.

It is interesting to note that, when no fan nor cuff was used, the pressure recovery on the front of the engine remained very nearly the same percent of free-stream impact pressure in climb as at high speed. This fact indicates that the flow through the cowling remained stable through the useful range of angles of attack.

The distribution of cylinder temperatures around the engine in the full-throttle level-flight condition is illustrated in figure 15. The values for each modification were taken from runs at approximately 18,500 feet density altitude. A study of figures 15 and 13 shows that the individual cylinder temperatures are more affected by other operating factors than by cooling-air pressures.

Tables I and II show that the lower cylinder temperatures were obtained where the available cooling pressures were also low. Figure 16 indicates that this effect is, at least in part, the result of small variations in the full-throttle power delivered by the engine for each

installation. The observed values of brake horsepower and of average cylinder-head temperature above free air are plotted against the product of the free-air density ratio and the pressure drop across the engine in inches of water. Figure 16 shows that the temperature varies with power at a given air flow. The differences in temperature are somewhat larger than would normally be expected from the amount of power variation at constant odp. It is probable that other factors, such as fuelair-ratio variations between tests and possibly variations in rotation and turbulence of the air stream, may also have affected the temperatures. The variations are not, however, large enough in relation to the experimental error to warrant evaluation of possible causes.

Ground Cooling

Time histories of representative temperatures observed during the ground-cooling runs are shown in figures 17 to 19 for the cowling without fan or cuffs, with cuffs 1, and with cuffs 2. It is immediately apparent that the ground cooling with either cuffs 1 or cuffs 2 is much improved over that obtained without fan or cuffs.

In no case were the cylinder head or barrel temperatures critical during the ground runs. Except in the case without fan or cuffs, cylinder temperatures were lower than for the high-speed condition.

In the test without fan or cuffs, the rear-spark-plug elbow of cylinder 11 slightly exceeded its limit of 248° F, after the engine had been cut off, when corrected to Army summer conditions. This elbow usually ran the hottest of the six measured on cylinders 1, 7, and 11. After cut-off in the ground run with the cuffs 1, however, the rear elbow temperature of cylinder 1 exceeded that of cylinder 11, as shown in figure 18.

The oil-in temperature also exceeded its limit of 185° F when corrected to Army summer conditions during the test without fan or cuffs.

CONCLUSIONS

- about 1 mile per hour less at the same power and altitude with the short-nose low-inlet-velocity cowling, without fan or cuffs, than with the long-nose high-inlet-velocity cowling and propeller cuffs. The use of propeller cuffs or a fan on the low-inlet-velocity cowling cost from 1 to 4 miles per hour in top speed. The axial-flow fan provided a higher cooling pressure than the cuffs for the same loss in speed.
- 2. The cooling-air pressure recovery on the front of the engine in the high-speed level-flight condition averaged 76 percent of free-stream impact pressure without fan or cuffs, 77 percent with propeller cuffs 2, 80 percent with propeller cuffs 1, and 84 percent with the axial-flow fan. Corresponding pressure recoveries in full-power climb at an indicated airspeed of 140 miles per hour were 74, 84, 84, and 97 percent free-stream impact pressure.

Langley Memorial Aeronautical Laboratory,
National Advisory Committee for Aeronautics,
Langley Field, Va.

REFERENCES

- Bailey, F. J., Jr., Johnston, J. Ford, and Voglewede, T.J.: Flight Investigation of the Performance and Cooling Characteristics of a Long-Nose High-Inlet-Velocity Cowling on the XP-42 Airplane. NACA A.R.R., April 1942.
- 2. Bailey, F. J., Jr., and Johnston, J. Ford: Flight Investigation of NACA D_S Cowlings on the XP-42

 Airplane. I High-Inlet-Velocity Cowling with Propeller Cuffs Tested in High-Speed Level Flight. NACA A.R.R., Jan. 1943.
- Johnston, J. Ford, and Voglewede, T. J.: Flight Investigation of NACA D_S Cowlings on the XP-42 Airplane. II Low-Inlet-Velocity Cowling with Axial-Flow Fan and Propeller Cuffs. NACA A.R.R., Jan. 1943.

XP-42 airplane	Test No Flight No. Run No.	/	2	3	22	5	/		8-2	_	5
Short-nose low- intet-velocity cowling With fan, without Cuffs	True Airspeed, mph. q., impact press., in. H. Atm. pressure, in. Hg. Atm. pressure, in. Hg. Ambient Air Temp., °F o, density ratio Density Altitude, ft. Rpm. Bhp. Manifold press., in. Hg.	36.5 17.10 4 .639 14500 935 40.2	35.2 16.50 -2 .624 15250	34.0 15.79 -3 .599 16500 2.68 873 37.6	32.2 15.16 -7 .580 17400 0 845 36.2	31.5 14.56 -9 .560 18500 812 34.8	35.4 17.22 9 .636 0/4650 925 40.4	332 34.9 16.56 7 614 15750 2 900	328 33.4 1591 1 598 16550 873 378	330 32,4 1529 -2 .576	326 309 14.64 -8 .561 18150 812 349
	Pre.	SSU	e r	atio	P	'gc					
Engine Pressure To	3-R 4-R 6-R Sheltered 7-R tubes 9-R behind 10-R engine	.37 .36 .39 .39 .40 .40	38 37 37 39 39 40 40	.37 .39 .39 .40 .40	.37 .36 .39 .39 .40 .40	.37 .37 .39 .39 .39 .39	.36 .38 .38 .39 .39 .39	.37 .36 .38 .38 .39 .39	.36 .35 .37 .37 .38 .38	36 38 38 39 39 39	36 36 38 38 39 39
5 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	14-R. 1-ED 3-EB 4-EB 6-ED Exhaust 7-EB side 05 9-EB barrel 10-EB	.86 .76 .83 .87 .84 .89 .89	.86 .77 .84 .86 .85 .89 .89	.86 .77 .83 .86 .84 .87 .89	.86 .89 .89 .89	.86 .77 .83 .86 .84 .88 .89	.85 .76 .82 .86 .83 .88 .89 .89	.85 .76 .83 .85 .83 .88 .88 .88	.84 .75 .81 .84 .83 .86 .87	36 .85 .76 .82 .85 .83 .88 .88	.85 .76 .83 .86 .84 .87 .88
Cylinder no. 1 I-TH I-IH I-EH O I-IB	14-EDJ 1-EH 3-EH 4-EH 6-EH 7-EH 9-EH 10-EH 12-EH 14-EH	.91 .80 .87 .83	.87 .85 .81 .90 .86 .84 .90 .42 .86	.84 .80 .90 .79 .86 .84 .90	80 91 79 86 84 91	.84 .80 .80 .80 .86 .85 .91	7	.80 .91 .79 .87 .85 .90 -92	83 18 90 .78 .85 .83 .90	86	.84 .80 .90 .79 .86 .84 .90
Sant Builton 1-E8 1-E8 1-E8 1-E8 1-E8 1-E8 1-E8 1-E8	1-TH 3-TH 4-TH 6-TH 7-TH 10-TH 10-TH	.84 .88 .83 .82	84 86 80 79 84 90 83 83 79	87 80 .79 .84 .89 .83	.80 .79 .85 .89 .84 .84	.85 .88 .83	.87 .80. .79 .85 .88 .82 .82	.86 .80 .79 .85 .87 .83 .83	.86 .80 .78 .84 .87 .82 .82	.83 .86 .80 .79 .84 .87 .83 .83	.86 .80 .79 .84 .89 .82
3-EH2 -0 3-EH -0 3-EH -0 3-EB -0 3-EB -0	1-IH Intake 6-IH bide of 10-IH head 1-ID Intake 6-ID side of 10-IB barrel 3-EH2 4-EH2 3-EB2 4-ED2	.88 .94 .83 .87 .87 .82 .88	.86 .88 .94 .84 .89 .89 .82 .88 .67	.88 .93 .84 .87 .88 .82 .87 .67	.88 .93 .83 .88 .88 .81 .88 .67	.87 .93 .84 .87 .88 .81	.88 .91 .83 .87 .88 .82 .82 .83	.88 .92 .83 .87 .88 .82 .87	.87 .91 .82 .87 .87 .81 .87	.85 .86 .92 .87 .88 .87 .88 .87 .78	.87 .92 .83 .87 .88 .81 .88

1	+									-
			9-21					9-20	0	
	/	2	3	4	5	1	2	3	4	5
Ind. airspeed, mph.	158	157	155	154	153	138	138	138	136	137
ge	12.4	12.2	11.9	11.8	11.7	9.5	9.4	9.4	9.2	9.3
Pressure altitude?	1		12300		19400-	2500-	8400-	13/00-	17100-	19700
Pressure altitude?	6400	8800	13300	17200	20000	3900	9500	14100	17800	20900
Av. free air temp, °F	25	24	12	-/	-11	31	25	10	-5	-10
	890	890	875		695	960	930		675	
Av. bhp.	400							364		
Av. manifold press.	400		54		30.0		25		21.1.	20.0
Rpm	-	d	340							
	AU	to.r.	ich, a	Int	,	F	ulla	ich, c	dimb	
			-			.:46				_
			With	101	, w	11110	W/ C	4113		
Pressur	er	otic	0, P/	190						
	1								-01	- 21
-	-22		-20		-/8	-28		-25		
	-20	-22	-20	15	-18	26		-26		
	-25	-26	-24	-21	22	33		-28		58
	09	-//	08	-09	-09	-16		-,15		-14
	08	//	07	-07	-09	-15	/2	-15	-14	-14
	08	7//	-,08	07	07	16	-15	15	-14	-14
	//	/2	-28	-07	07	-/7	14	-15	-15	-14
	-20	-20	-/8	-15	16	-26	-26	-25	-24	-24
	22	-22	-21	-18	-18	-30	-26	-25	-26	-26
	.97	.91	.95	,93	92	1.03	99	95	.20	87
	.69	.73	.7/	.73	.72	.75	77	21	.74	21
	.97	96	90	88	89	97	1.02	92	90	.87
	112	108	101	99	99	1.27	1.15	106	1.04	100
	1.07	99	.98	.96	97	1.00	1.09		96	.76
	1.06	1.01	1.02	105	1.03	1.11	409	1.04	102	102
	1.04	1.00	1.03	99	1.01	1.10		1.04		.99
	99	96	99	99	.97	1.07	1.02	99	96	92
	1.05	1.05	101	99	.97	1.13	1.04		.98	.94
	90	94	90	91	.88	1.01	95	.89	.89	.88
~	.86	86	.79	78	78	.88	91	80	.799	.78
	1.16	1.17	1.05	101	1.01		1.19	1.10	1.09	
	.88	93	.81	.82	80	.98	96	.86	.81	.79
		97	.99	.96	97		1.09	99	99	95
	1,00			.92	91	.99	97	94	90	.87
	90	.86	1.08		1.04			1.14		
	1.07	1.08		1.06				1.13		1.11
<u>.</u>	1.09	1.10		1.10	1.06					
	1.11	1/2	106	1.03	99		-	.96	and the same of	but ded.
140	1.01	.99	.97	96	91		1.03		.95	92
	.98	.97	.92	90	89		1.00	94	9/	20
	.94	.89	.86	.84	83	.98	.94	.87		.83
	.89	.94	.84	86	83	.97	95			.83
-	101	.99	1.01	.95	94	1.07	1.12	1.01		.94
*	1.02	.99	1.03	1.05	103	1.18	1.14		1.02	
7	.87	.88	87	.88	.88	1.01	94	90	.87	
	.90	94	.88	.92	90	1.08	.99	.94	.91	90
	.89	.92	.84	85	85	1.08		91	.87	.86
	1.02	1.03	.97	.95	95	1.05	1.03	.97	97	91
	114	112	1.05	1.05	1.03	1.22	1.18	110	1.05	1.02
	118	1.14	108	110	1.09	1.34	1.24	1.16	112	1.10
	.91	.87	92	90	.89	1.00	.95	.90	.89	.84
	1.06		1.03	1.00	1.00		1.13	1.10	1.05	96
	1.02	1.03	1.00	1.01	.98	1.16	1.11		1.00	99
	.81	83	.79	.76	78	69	.84	74	77	.74
	1.12	1.05	98	.96	95	1.17		1.02		96
	47	48	.48	.49	51	48		.53	49	46
							.98			.86
	.86	.83	.8/	.83	.83	90	.70	.00	01	00
	-			-	-	-				

Table 16). - (continued)

VP-42 21-1-	Tant No FI LA M	// / / / / / /
XP-42 Airplane	Test No Flight No. Run No.	1 2 3 4 5 1 2 3 4 5
SHOrt-Mose low- Inlet-Velocity Cowling	True Airspeed, mph.	
No fan, no cuffs	Atm. pressure, in Hg. Ambient Air Temp, °F o, density ratio	17.18 16.70 15.84 15.18 14.54 16.46 15.81 15.17 14.53 13.9 15 12 6 1 -2 2 2 -4 -5 -1 16.28 .614 .590 .571 .552 .618 .594 .577 .555 .53
	Density Altitude, ft. Rpm.	15050 5700 6950 7950 8950 5500 6750 7650 8800 200 2680 2650
	Bhp. Manifold press., in tig.	871 857 834 810 794 860 832 803 780 75 39.2 37.7 36.4 35.1 33.9 37.7 36.5 35.1 33.8 32
		High Speed High Speed
		Pressure ratio, Mac
Engine Pressure Tube Locations	1 -R 3 -R 4 -R Sheltered	.29 .29 .29 .29 .29 .30 .30 .30 .30 .2 .39 .28 .28 .28 .28 .29 .29 .29 .29 .20
cyl.	6-R tubes 7-R behind	28
360 0 0 13	9-R engine	33 .32 .33 .32 .33 .33 .33 .34 .3. .33 .33 .32 .33 .32 .33 .33 .33 .34 .3.
4 000000	12-R 14-R	31 30 30 31 30 31 71 31 31 31 3 29 29 29 29 28 30 30 29 30 2
of the date	1-EB 3-EB	80 .80 .79 .79 .79 80 .81 .81 .80 .81 68 .68 .68 .67 .68 .68 .68 .67 .68 .68
	4-EB Exhaust	69 .69 .69 .70 .69 .69 .69 .69 .69 .69 .69 .69 .69 .69
7 8 29	7-EB side of 9-EB barrel	18
	10 - EB 12 - EB 14 - EB	30 .80 .80 .79 .80 .80 .81 .82 .80 .80 .76 .76 .75 .75 .75 .76 .77 .77 .78 .79
Cylinder no. 1	1-EH 3-EH	80 .79 .80 .79 .80 .82 .82 .82 .81 .80 80 .79 .79 .79 .79 .80 .81 .79 .79 .79 .73 .74 .73 .73 .73 .73 .72 .73 .73 .73
1-TH 1-ZH	4-EH Exhaust	76 .75 .74 .73 .75 .75 .74 .74 .74 .74 .74 .73 .73 .73 .73 .73 .73 .73
locations of the total of the t	7-EH side of	.8/ .80 .80 .80 .80 .81 .81 .81 .80 .80 .77 .77 .77 .77 .78 .78 .78 .78 .78 .78
\$ 0. 1-1B	10-EH 12-EH	81 .81 .81 .81 .81 .81 .82 .83 .82 .83 .76 .76 .75 .76 .75 .77 .78 .77 .77 .7
1-18 1-18	14-EH) 1-TH	79 79 78 78 78 79 80 79 80 79 - 80 80 80 79 81 80 80 80 79
() ← /-R	3-TH 4-TH	75 .76 .76 .75 .76 .75 .76 .74 .74 .69 .69 .69 .88 .69 .68 .69 .68 .69 .68 .69 .70 .66
6.	6-TH Top of 7-TH head	.69 .69 .68 .69 .68 .70 .68 .69 .69 .69 .69 .79 .78 .78 .78 .78 .79 .78 .78 .79 .78 .78 .79 .78 .79 .79 .79
Cylinder no. 3	9-TH 10-TH 12-TH	8/ 8/ 8/ 82 82 82 82 82 82 82 8 73 72 73 74 74 74 74 74 74 77
3-EH2	14-TH) 1-IH) Intake	73 73 73 74 74 74 75 74 75 7 7/ 7/ 70 72 72 71 72 72 72 72 72 72 72 72 72 72 72 72 72
0 0 3-EH → 0	6-IH side of	78 .78 .79 .78 .78 .79 .79 .79 .79 .79 .81 .80 .81 .82 .80 .82 .81 .81 .81 .81 .81 .82 .84 .84 .85 .85 .85 .85 .85 .86
Botto 3-EB-0	1-IB Intake 6-IB side of	76 .77 .76 .76 .75 .76 .77 .77 .77 .77 .81 .81 .81 .80 .80 .81 .82 .83 .81 .80
3-EB2-0	10 - 1B) barrel 3 - EH2	78 78 78 79 78 80 80 79 80 79 74 .74 .73 .73 .74 .73 .73 .73 .73
0= 3-R	4 - EH2 3 - EB2	.74 .73 .72 .72 .72 .72 .72 .73 .73 .73 .74 .56 .55 .56 .56 .57 .60 .59 .60 .60 .59
	4 - EB2	.60 .59 .60 .61 .61 .59 .58 .60 .59 .5

	_	4-01	Parity						
			1-2	,	1		10-3		_
	/	2	3	4	/	2	3	4	5
Ind. airspeed, mph	156	154	154	152	/39	141	137	138	/37
Qc	1	11.6			9.5		9.2	9.4	9.2
Pressure altitude	5000	9300	14900	18800	8200	9900	13300	15500	18800
range, ft					1				_
Av. free air temp, "F Av. bhp	20	920	970	720	920	890	7	700	600
Av. manifold press.		39.8						33.4	
Rpm	4	251		-	4	-25		-	-
	0.4			4	-	# 1		d b	
	PH.O.1	O. ric			FUI			KINI K	_
		/	10 1	011,	100	-011	3		
Pressure ra	+10,	P/q	le .						
	-26	28	-26	26	-33	-33	-34	-36	-34
	-26	-26	-26	24	-30		-34	34	-30
	32	-31	-31	3/	-36	37	38		38
	-20	20		-17	21	-24	24		-24
,	18	/7	17	/7	22	21	-24		24
	-20	/7	-17	-17		24	-24		:24
·	26	-26	-26	-26	33	33	-,34.	-34	-34
	29	-28	:29	-26	-34		The same of		-36
	80	.77	.75	.73	.75	.76	.73	.70	.73
	.55	67	.58	.58	.60	.58	.59	.58	.59
	79	.83	.80	.82	.79	.77	.77	.76	.77
	.76	.77	.77	.77	.76	.77	73	.71	.73
	.88	.86	.86	.83	.86	83.	.80	.79	.80
	.88	.88	.88	.87	.86	.86	.85	.86	.83
- To	.79	.86	.82	76	.88	.89	.79	.85	.86
	.7/	.77	.73	.71	.73	.73	.72	21	70
	.59	.64	.58	.59	.65	.60	-58	.56	.54
	.73	.78	.73	.71	.74	.76	.72	.68	.70
	67	.65	.65	.63	.63	.63	.58	.56	.59
	.84	.83 .78	.82	.76	.79	.78	78	.77	.76
	.88	.90	.85	84	94	91	.89	85	.85
	.90	.93	.89	.88	.97	97	97	.96	97
	.79	.80	.75	76	.83	.79	.80	.81	.80
	.78	.82	75	.76	.81	.79	.75	.72	.73
	.75	.78	.7/	.70	.77	.75	.73	.55	.68
1	.68		.64	63	.67	.64	.59	.56	.59
	.82	.82	82	81			.85	.79	.78
			.88	.85	.92		.87	.86	.87
*	.75		74	.73	.75	.74	74	.74	.74
	.50		.72	.73	.76	.76	.62	.73	.77
	.79		.75	76	.78	79	.77	.75	.74
	.86		84	.85	.88		.85	.80	.83
				.93	.98	.98	95	94	92
	.73	.72	.72	.71	.74	.72	.74	.71	.72
			84	.83				.84	.84
			.62	.84					.88
4 770 1				.68	.74			.68	.66
			.30	.30			29	.29	.29
	.52	.66	58	.61	.62	.59	56	.53	.54
			-				-	-	

VD 1	2 2 2 2 2 2	Test Na - Flight No.	12-1	4 5	12-2	
	2 airplane -	Run No.	1 2 3	4 5	1 2 3	7 3
	t-nose low-inlet- city Cowling	True Airspeed, mph. qe, impact press., in. H. C. Atm. pressure, in. Hg. Ambient Air Temp., °F o, density ratio Density Altitude, ft. Rpm. Bhp. Manifold press., in. Hg.	35.5	32,7 31.8 15.11	89/ 873 850 38.9 37.4 36./	31.1 30. 14.54 13.9 1 -5 548 .53. 19150 200
			-	- High .	speed	
		/		Cull	1, 10 1411	
	3		Pre	ssure r	ratio, P/g.	
E	ngine Pressure Tube	1-R	32 32 . 32	.32 .32	32 32 31	.32 .33
	Locations	3-R	32 .31 .30			.31 .32
		4-R shaltered		.31 .30		.31 .32
	cy/.	1-R behind		.33 .33		34 3
	2 0 /4	9-R engine	35 .35 .34	36 .34	.35 .35 .34	.35 .3
	300 13	10-R	35 ,35 ,34	.36 .34	.35 .35 .34	
		12-R 14-R)	33 .33 .32 33 .32 .32	.33 .33	.33 .33 .32	.33 .3 .32 .3
	4	1-EB)	82 .82 .82	.82 .81		.83 .8.
	of I	3-EB	72 .71 .70	.72 .71		.73 .7
·	No re elegan	4-EB	74 73 73	.73 .73	74 74 74	.74 .7
	69/10	6-EB exhaust	85 84 83 80 80 80	.83 .84		.81 .8
	2 2	9-EB barrel	85 .84 82	.83 .83	.84 .84 .83	
	8	10-EB	86 .86 .85	85 85	.86 .87 .86	.86 .8
		12-EB	.78 .78 .77	.78 .77		78 .7
	Cylinder no. 1	14-EB) 1-EH)	<u>84 .84 .83</u> 82 .81 .81	.82 .81	.84 .84 .84 .82 .82 .82	.86 .8
		3-EH	.79 .78 .77	.78 .78		.79 7
	I-TH	4-EH	83 .82 .82	.83 .81	.83 .83 .83	.82 .8
200	I-EH.	6-EH exhaust	.79 78 .77	.78 .76	.78 .79 .78	.78 %
ocations	0	9-EH side of	84 .84 .83	.80 .80		.80 .8
20		10-EH		.87 .86		.87 .8
9	1-18	12-EH	79 .77 .78	.80 .79		.79 .7
50	1-EB	14-EH)	.83 .82 .82	.83 .82		.82 .3
oylinders		1-TH)	.83 .82 .82 81 .81 .80	.83 .8.2	.80 .80 .80	.82 .8
-20	04 1-R	4-TH	.76 .76 .75		.76 .76 .75	
8 8		6-TH top of	76 .74 .74	.74 .74		.75 .7
6.	01: 1:	7-TH head	83 .82 . 82 8 4 .85 . 83	.82 .82	.82 .84 .82 .84 .85 .85	.82 .8
designating typical cylii	Cylinder no. 3	9-TH	76 .76 .76	.77 .77		.78 .7
3 0	3-74-40	12-TH	76 .76 .76	.76 .77	.76 .77 .77	.77 .7
	3-EH2 -0	14-TH)	75 .74 .75	.74 .75	78 76 77	.76 .7
For	3-EH	1-IH intake		.86 .86	.81 .82 .81 .87 .88 .87	.86 .8
26	0 - " - 0	6-IH side of	86 .85 .86	91 90		92 9
Method	250,0	1-18) intake	79 ,79 .79	.79 .78	79 .80 .79	.79 .7
0	3-£8	6-IB side of	87 .87 .86	.86 .85		.86 .8
	9-682-00	10-18) barrel	84 84 83	.84 .83	84 84 84	.85 .8
		3 - EH2 4 - EH2	80 .79 .79	.79 .78	78 .79 .78 .80 .82 .80	.79 .7
	04-3-R	3 - EB2	62 .61 .60	62 62		.63 .6
		4 - EB2	67 .64 .66	66 .64	.67 .68 .66	.65 .6

13-1 13-2 13-3 13-2 13-2 13-2 13-2 14-2 3 4 12-3 4 12-3 4 12-3 4 12-3 4 12-3 4 12-3 4 12-3 4 12-3 13-1 138 137 138 137 138 137 138 137 138 137 138 137 138 137 138 137 138 137 138 137 138 137 138 137 138 137 138 137 138 137 138 137 138 137 138 137 138 138 137 138 138 137 138 138 137 138 138 137 138 138 137 138								-						
Ind airspeed mph 12 3 4 5 12 2 3 4 2 3 4 2 3 4 Pressure altitude		100	-	13-1				13	-3			13	-2	
11nd airspeed mph 141 158 158 154 157 138 140 137 137 138 138 137 138 138 137 138 138 137 138 138 137 138 138 137 138 138 137 138 138 137 138 138 137 138 138 137 138 138 137 138 138 137 138 138 137 138 138 137 138 13		1			-	5	1			4	1	2	3	4
9:		1												100
9:	Ind airspeed mph	161	158	158	154	157	138	140	137	137	138	138	137	138
Pressure affiliate											1			
Av. Bhp. Se	Pressure altitude										1			
Av. Bhp. Se	range ff													
Av. monifold press. 380 386 384 337 302 387 385 335 300 477 372 32.1 291- 25 4 0 Auto. rich climb														
Av. manifold piress. 380 386 384 387 382 397 385 335 380 417 372 321 291 400 7 100 7											1			
Auto. rich climb Auto. rich_climb Full rich_climb Cuff 1,		840	880	860	770	700	915	890	780	100	910	793	000	380
Auto. rich climb Auto, rich, climb Full rich, climb	Av. manifold press.	39.0	39.6	38.4	33.7	30.2	39.7	38.5	33.5	30.0	417	37.2	32.1	29.1-
Culff 1,	Rpm	4	— 2	540) —		4			25	20			
Culff 1,		10,		,	4	_	0			1 6	-	,	1 1	
Pressure rotio, he -33 -32 :30 -27 -28 -33 -36 -37 -37 -37 -34 -36 -36 -36 -36 -36 -36 -36 -36 -36 -36		HUTE	o. r.1	cne	iim	D	HUI	0,110	n,ci	umo	FUI	rie	n, csi	mp
Pressure rotio, he -33 -32 :30 -27 -28 -33 -36 -37 -37 -37 -34 -36 -36 -36 -36 -36 -36 -36 -36 -36 -36		-				CU	ff	1,	ho	fai	7	_		->
-33 -32 -30 -27 -28 -33 -36 -37 -37 -36 -36 -36 -37 -36 -36 -36 -36 -36 -36 -36 -36 -36 -36		-							`					
-33 -32 -30 -27 -28 -33 -36 -39 -39 -39 -36 -36 -36 -39 -36 -36 -36 -36 -36 -36 -36 -36 -36 -36		1		PI	ess	ure	roti	0. P	20					
-30 -28 -28 -28 -28 -28 -28 -31 -33 -34 -36 -36 -36 -36 -36 -37 -37 -37 -37 -37 -37 -37 -37 -37 -37							,	-, ,,						
-35 34 :38 -32 -31 36 -38 -39 41 35 -38 -31 41 -41 -19 -17 -16 -16 -16 -16 -20 -21 -24 -24 -24 -27 -26 -26 -24 -24 -27 -26 -26 -24 -28 -24 -22 -24 -28 -24 -22 -24 -28 -24 -22 -24 -28 -24 -22 -21 -24 -28 -21 -21 -21 -19 -18 -16 -22 -23 -24 -26 -26 -22 -24 -25 -26 -22 -27 -23 -27 -27 -27 -27 -27 -27 -27 -27 -27 -27		33	-,32	-30	-29	-28	33	-36	39	-39	34	36	36	-39
-35 34 :38 -32 -31 36 -38 -39 41 35 -38 -31 41 -41 -19 -17 -16 -16 -16 -16 -20 -21 -24 -24 -24 -27 -26 -26 -24 -24 -27 -26 -26 -24 -28 -24 -22 -24 -28 -24 -22 -24 -28 -24 -22 -24 -28 -24 -22 -21 -24 -28 -21 -21 -21 -19 -18 -16 -22 -23 -24 -26 -26 -22 -24 -25 -26 -22 -27 -23 -27 -27 -27 -27 -27 -27 -27 -27 -27 -27														
-19 -17 -16 -16 -16 -16 -20 -21 -24 -24 -19 -21 -26 -26 -19 -17 -16 -16 -16 -20 -20 -20 -24 -24 -24 -20 -22 -24 -24 -27 -27 -27 -27 -27 -27 -27 -27 -28 -24 -22 -24 -24 -27 -27 -27 -27 -27 -27 -27 -27 -27 -27										,				
-19 -17 -16 -16 -13 -20 -20 -24 -24 -20 -22 -24 -24 -21 -21 -19 -19 -15 -16 -22 -23 -24 -24 -22 -24 -22 -24 -22 -24 -21 -21 -19 -18 -16 -22 -23 -24 -24 -25 -26 -26 -22 -24 -24														
-21 - 19 - 19 - 18 - 16 - 22 - 23 - 24 - 24 - 23 - 24 - 24 - 23 - 24 - 24														
-21 -21 -19 -18 -16 -24 -27 -26 -26 -24 -24 -26 -26 -32 -32 -32 -30 -30 -39 -39 -30 -36 -36 -39 -39 -34 -36 -35 -39 -39 -32 -35 -35 -39 -39 -35 -35 -39 -35 -35 -39 -35 -35 -39 -35 -35 -39 -35 -35 -39 -35 -35 -39 -35 -35 -39 -35 -35 -39 -35 -35 -35 -35 -35 -35 -35 -35 -35 -35														
-32 -32 -30 - 29 - 28 - 36 -36 -36 -39 -39 -34 -36 -35 -39 -32 -29 -30 -28 -26 -36 -36 -36 -36 -39 -38 -35 -39 -35 -36 -35 -39 -38 -36 -35 -39 -38 -35 -39 -38 -35 -39 -38 -35 -39 -38 -35 -39 -38 -35 -39 -38 -35 -39 -38 -35 -39 -38 -35 -39 -38 -35 -39 -38 -35 -39 -38 -35 -39 -38 -36 -35 -39 -38 -36 -35 -39 -38 -36 -35 -39 -38 -36 -35 -39 -38 -36 -36 -36 -36 -39 -39 -38 -36 -36 -30 -30 -30 -35 -39 -30 -35 -39 -30 -35 -39 -30 -35 -39 -30 -35 -39 -30 -35 -39 -30 -35 -39 -30 -35 -39 -30 -35 -39 -30 -36 -36 -30 -30 -30 -30 -30 -30 -30 -30 -30 -30										2-4	-			
-32 -29 -30 -28 -36 -36 -36 -36 -36 -33 -36 -35 -35 -35 -36 -35 -39 -39 -39 -39 -39 -39 -39 -39 -39 -39						1.0								
78 82 79 32 78 82 83 78 73 83 80 75 74 58 63 42 65 62 66 65 61 61 68 63 60 60 65 67 66 66 65 70 66 66 45 70 66 64 70 70 64 66 87 86 88 90 88 97 88 90 90 90 95 97 91 88 85 87 86 88 90 88 97 88 90 90 90 95 97 91 88 85 87 86 88 90 88 100 36 97 88 85 99 95 88 24 92 86 88 90 88 90 90 90 90 90 90 90 90 98 88 24 84 90 84 86 84 99 99 91 88 100 93 88 33 80 81 81 84 80 75 77 74 78 78 18 80 90 93 88 33 80 81 84 80 78 88 71 66 62 65 71 66 66 81 73 71 75 70 66 71 78 77 70 70 70 66 76 70 77 77 77 77 75 70 66 71 78 77 79 77 70 70 70 66 76 70 77 77 77 77 77 70 70 70 66 70 77 77 77 77 77 77 70 70 70 70 70 70										200				
58 .63 .62 .65 .66 .65 .61 .61 .68 .63 .60 .60 .60 .65 .61 .61 .68 .63 .60 .60 .65 .67 .66 .66 .65 .70 .66 .66 .64 .70 .70 .64 .66 .65 .70 .66 .66 .65 .70 .66 .66 .64 .70 .70 .64 .66 .87 .70 .64 .66 .87 .70 .64 .66 .87 .70 .64 .66 .87 .70 .64 .66 .87 .70 .87 .70 .64 .66 .87 .70 .70 .70 .87 .70 .87 .70 .70 .70 .70 .87 .70 .70 .70 .70 .70 .70 .70 .70 .70 .7		52	-24	30		-20th			100			36		
65 67 66 66 65 70 66 66 64 70 70 64 66 87 70 70 64 66 87 87 86 87 80 80 80 85 87 81 82 82 86 83 87 88 80 80 80 80 80 80 80 80 80 80 80 80		.78												.74
87 .86 .89 90 .88 97 88 90 90 \$\frac{1}{95}\$.97 91 88 95 .85 .87 86 .86 .83 .99 87 .88 .85 .99 95 .88 .84 92 .86 .88 .90 .88 .103 96 94 90 100 97 .96 98 .84 .85 .89 .88 .85 .89 .88 .84 .89 .84 .80 .84 .80 .84 .80 .87 .90 .82 .78 .81 .80 .83 .80 .81 .84 .80 .87 .90 .82 .78 .91 .83 .85 .77 .86 .84 .80 .81 .84 .80 .78 .88 .77 .78 .80 .85 .83 .77 .78 .80 .81 .84 .80 .78 .88 .77 .78 .80 .81 .84 .80 .78 .88 .77 .78 .78 .80 .81 .84 .80 .78 .88 .77 .78 .86 .85 .83 .77 .75 .70 .66 .71 .72 .71 .77 .70 .70 .66 .71 .74 .72 .80 .75 .79 .77 .74 .85 .85 .83 .77 .75 .70 .66 .71 .72 .71 .77 .70 .70 .66 .74 .77 .72 .71 .77 .70 .70 .70 .86 .73 .74 .89 .89 .89 .89 .97 .97 .97 .97 .97 .97 .97 .97 .97 .9														
.85 .87 .86 .86 .83 .99 .87 .83 .85 .99 .95 .88 .46 .88 .90 .88 .103 .96 .94 .90 .101 .97 .96 .88 .20 .88 .80 .87 .99 .91 .96 .98 .101 .97 .96 .98 .101 .97 .96 .98 .101 .97 .96 .98 .101 .97 .96 .98 .101 .97 .96 .98 .101 .97 .96 .98 .101 .97 .96 .98 .101 .97 .96 .98 .101 .97 .91 .37 .78 .30 .88 .37 .78 .30 .87 .38 .37 .79 .77 .74 .72 .80 .82 .37 .79 .77 .74 .72 .80 .82 .82 .82 .82 .82 .87 .77 .77 .74 .72 .80 .82 .82 .87 .97 .97 .70											-			17.0
92 36 88 90 88 1,03 96 94 90 1,01 97 96 38 1,01 97 96 58 1,01 59 58 52 38 38 90 38 1,00 93 38 37 77 74 77 74 77 74 77 76 76 78 37 77 77 74 77 70 70 66 71 72 77 70 70 66 71 72 77 78 78 32 21 97 97 97 99 95 1,09 85 <td></td> <td>.87</td> <td>.86</td> <td>.89</td> <td>.90</td> <td>.88</td> <td>.97</td> <td>.88</td> <td>.90</td> <td>.90</td> <td>.95</td> <td>.97</td> <td>.91</td> <td>.89</td>		.87	.86	.89	.90	.88	.97	.88	.90	.90	.95	.97	.91	.89
		.85	.87	.86	.86	.83	.99	.87	.88	.85	.99	95	.88	84
84 90 84 86 84 99 99 91 88 100 93 88 83 80 81 81 84 30 37 90 82 78 91 83 84 77 69 78 77 30 75 79 77 74 72 80 76 71 71 66 67 68 69 66 71 66 62 62 52 62 52 62 52 62 52 80 81 84 80 78 87 70 70 70 70 66 76 75 77 70 66 71 72 71 77 70 70 70 66 76 73 71 74 81 85 82 85 82 91 90 85 83 89 84 83 82 97 97 97 97 99 95 109 100 101 99 11 101 97 92 87 81 85 84 86 87 84 92 88 89 87 78 89 84 83 82 97 101 101 101 103 51 15 115 117 766 119 117 100 100 85 84 86 87 84 92 88 82 79 77 84 82 77 74 76 81 81 81 81 78 84 76 75 76 82 82 71 70 91 97 94 93 85 100 108 98 98 98 92 96 92 96 92 106 108 100 98 108 97 91 88 92 96 92 96 92 106 108 100 98 108 97 91 88 92 96 92 96 92 106 108 100 98 108 97 91 88 92 96 92 96 92 106 108 100 98 108 97 91 88 92 96 92 96 92 106 108 100 98 108 97 91 88 92 96 97 97 97 97 97 109 108 100 109 97 78 83 83 84 83 85 82 84 80 77 77 78 87 88 90 84 82 78 83 83 84 83 85 100 108 100 98 108 97 91 88 92 96 92 96 92 106 108 100 98 108 101 98 95 73 76 76 78 78 77 82 84 80 77 78 83 76 76 74 78 83 83 84 83 95 93 92 89 90 84 82 70 71 72 73 74 74 75 73 74 77 74 75 75 76 76 76 74 78 83 83 84 83 95 93 92 86 99 100 87 91 88 92 96 92 96 92 100 108 100 98 108 101 98 95 73 76 77 78 98 93 97 94 92 100 108 100 100 100 100 100 100 100 100		92	.86	.88	.90	.88	1.03	96	94	90	1.01	97	96	92
80 81 81 84 50 57 90 82 78 91 83 84 77		.72	94	94	.91	.89	1.01	97	.96	94	1.01	.99	98	95
.69 .78 .77 .80 .75 .79 .77 .74 .72 .80 .76 .71 .71 .66 .67 .68 .69 .66 .71 .66 .62 .62 .52 .32 .64 .62 .59 .80 .81 .84 .80 .78 .88 .77 .78 .76 .85 .83 .77 .75 .70 .66 .71 .72 .71 .77 .70 .70 .66 .71 .72 .71 .77 .70 .70 .66 .74 .73 .71 .69 .92 .91 .92 .90 .86 .103 .95 .91 .91 .101 .97 .92 .87 .83 .82 .85 .82 .85 .82 .87 .97 .97 .97 .97 .97 .99 .95 .109 .100 .00 .99 .1.11 .103 .98 .98 .97 .101 .101 .101 .101 .95 .1.15 .1.15 .1.17 .106 .1.19 .1.17 .100 .108 .85 .84 .86 .87 .84 .85 .82 .89 .87 .94 .89 .83 .76 .82 .82 .84 .85 .82 .84 .85 .82 .87 .79 .77 .84 .82 .77 .74 .76 .81 .81 .81 .81 .81 .78 .84 .76 .75 .78 .82 .82 .82 .76 .78 .70 .73 .76 .76 .74 .77 .69 .73 .71 .80 .72 .72 .70 .91 .97 .94 .93 .85 .108 .88 .95 .89 .108 .10 .98 .95 .73 .76 .75 .78 .78 .84 .80 .72 .72 .70 .91 .97 .94 .93 .85 .89 .89 .108 .101 .98 .95 .73 .76 .75 .78 .78 .78 .84 .83 .83 .84 .83 .95 .93 .92 .88 .89 .90 .84 .82 .76 .78 .78 .84 .83 .83 .84 .83 .95 .93 .92 .88 .89 .90 .84 .82 .70 .77 .78 .88 .83 .83 .84 .83 .95 .93 .92 .88 .89 .90 .84 .82 .70 .77 .78 .78 .83 .83 .84 .83 .95 .93 .92 .88 .89 .90 .84 .82 .70 .76 .76 .76 .76 .76 .76 .76 .77 .77 .77		.84	90	.84	86	.84	.99	99	91	.88	1.00	.93	.88	.83
.66 .67 .68 .69 .66 .71 .66 .62 .62 .62 .62 .62 .62 .59 .80 .81 .84 .80 .78 .88 .71 .78 .76 .85 .83 .71 .75 .70 .66 .71 .72 .71 .71 .70 .70 .66 .74 .72 .71 .69 .92 .91 .92 .90 .86 .103 .95 .91 .91 .101 .97 .92 .87 .81 .85 .83 .82 .97 .97 .97 .97 .97 .97 .97 .97 .97 .97		80	81	.81	84	.80	.87	90	.82	.78	91	.83	.84	77
.80		.69	.78	.77	.80	.75	.79	.77	74	.72	.80	.76	71	7/
70 .66 71 .72 .71 .77 .70 .70 .66 .76 .73 .71 .69 92 .91 .92 .90 .86 .103 .95 .91 .91 .101 .97 .92 .87 -81 .85 .82 .85 .82 .91 .90 .85 .83 .89 .84 .83 .82 97 .97 .97 .99 .95 .109 .100 .101 .99 .1.11 .103 .98 .98 -97 .101 .1.01 .101 .55 .1.5 .1.5 .1.15 .1.17 .106 .1.19 .1.71 .100 .428 -85 .84 .86 .87 .84 .92 .88 .89 .87 .94 .82 .77 .74 -76 .81 .81 .81 .81 .81 .78 .84 .76 .75 .75 .82 .82 .74 .71 -70 .73 .76 .76 .74 .77 .70 .73 .73 .74 .80 .74 .71 .70 -91 .97 .94 .93 .85 .108 .98 .95 .89 .108 .97 .91 .88 -92 .96 .92 .96 .92 .106 .108 .100 .98 .108 .101 .98 .95 -73 .76 .75 .78 .77 .82 .84 .80 .77 .83 .76 .67 -78 .83 .83 .84 .83 .95 .93 .92 .88 .90 .84 .82 -70 .67 .66 .69 .65 .74 .71 .77 .73 .83 .76 .67 .64 -78 .81 .84 .80 .81 .87 .81 .80 .80 .80 .80 .84 .80 .76 -78 .81 .84 .80 .81 .87 .81 .80 .80 .80 .80 .84 .80 .76 -78 .81 .84 .80 .81 .87 .81 .80 .80 .80 .80 .84 .80 -72 .72 .70 -73 .76 .76 .76 .74 .77 .97 .97 .97 .101 .101 .104 .99 -72 .78 .75 .76 .73 .80 .79 .74 .71 .73 .83 .76 .67 .64 -78 .81 .84 .80 .81 .87 .80 .80 .80 .80 .80 .84 .80 .76 -93 .93 .93 .97 .94 .92 .104 .95 .98 .96 .99 .101 .100 .104 .99 -72 .78 .75 .76 .73 .80 .79 .79 .79 .701 .101 .104 .99 -72 .78 .75 .76 .73 .80 .79 .79 .79 .701 .101 .104 .99 -72 .78 .75 .76 .73 .80 .79 .79 .79 .101 .100 .104 .99 -72 .78 .75 .76 .73 .80 .79 .79 .79 .101 .100 .104 .99 -72 .78 .75 .76 .73 .80 .79 .79 .79 .101 .100 .104 .99 -72 .78 .75 .76 .73 .80 .79 .79 .79 .101 .100 .104 .99 -72 .78 .75 .76 .73 .80 .79 .79 .79 .101 .99 .97 .101 .100 .104 .99 -72 .78 .75 .76 .73 .80 .79 .79 .79 .101 .100 .104 .99 -72 .78 .75 .76 .73 .80 .79 .79 .79 .101 .100 .104 .99 -72 .78 .75 .76 .73 .80 .79 .79 .79 .79 .101 .100 .104 .99 -72 .78 .75 .76 .73 .80 .79 .79 .79 .79 .101 .100 .104 .99 -72 .78 .75 .76 .73 .80 .79 .79 .79 .101 .100 .104 .99 -72 .78 .75 .76 .73 .80 .79 .70 .70 .70 .70 .70 .70 .70 .70 .70 .70		.66	.67	.68	.69	.66	.71	.66	62	.62	72	.64	62	.59
\$\begin{align*} \begin{align*} \begin{align*} \begin{align*} \begin{align*} \begin{align*} \begin{align*} \begin{align*} \begin* \begin{align*} \begin* \begin		.80	.81	.84	.80	.78	.88	.77	.78	76	.85	.83	.77	.75
\$\begin{align*} \begin{align*} \begin{align*} \begin{align*} \begin{align*} \begin{align*} \begin{align*} \begin{align*} \begin* \begin{align*} \begin* \begin		.70	.66	71	.72	.71	.77	.70	.70	.66	.76	.73	7/	.69
\$\begin{align*} \begin{align*} \begi				92	90				91		101	07		
97 97 97 97 99 95 1.09 1.10 1.01 99 1.11 1.03 98 98 1.97 1.01 1.01 1.01 1.01 95 1.15 1.15 1.11 7.06 1.19 1.17 1.00 1.28 1.85 8.4 8.6 8.7 8.4 9.2 8.8 8.9 8.7 94 8.8 83 .76 1.6 81 81 81 81 88 1.78 8.4 7.6 7.5 7.5 8.2 8.2 8.2 7.7 7.4 7.0 1.73 4.9 7.4 7.6 7.3 7.6 7.6 7.4 7.7 4.9 7.3 7.1 80 7.4 7.1 7.0 1.73 4.9 7.4 7.6 7.3 7.8 7.4 7.1 8.0 7.4 7.1 7.0 1.73 4.9 7.4 7.6 7.3 7.8 7.8 7.8 7.8 80 7.4 7.1 7.0 1.9 1.9 1.0 1.0 1.9 1.9 1.0 1.9 1.9 1.9 1.9 1.0 1.9 1.9 1.9 1.9 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0	-													
\$\begin{align*} \begin{align*} \begi														
.85 .84 .86 .87 .84 .92 .88 .87 .94 .88 .87 .94 .88 .83 .76 .76 .82 .84 .85 .82 .84 .82 .79 .77 .64 .82 .77 .74 .74 .76 .78 .84 .76 .75 .75 .82 .82 .76 .72 .70 .73 .71 .80 .74 .71 .70 .73 .71 .80 .74 .71 .70 .73 .71 .80 .74 .71 .70 .73 .71 .80 .74 .71 .70 .73 .71 .80 .74 .71 .70 .73 .71 .80 .74 .71 .70 .73 .71 .80 .74 .71 .68 .80 .72 .72 .70 .93 .82 .89 .80 .87 .91 .88 .92 .90 .89 .90 .89 .95 .93 .92 .88 .98 .90 .84 .82 .		2000												
.82 .82 .84 .85 .82 .84 .82 .79 .77 .84 .82 .77 .74 .76 .81 .81 .81 .78 .84 .76 .75 .75 .82 .82 .76 .78 .70 .73 .76 .76 .74 .77 .69 .73 .71 .80 .74 .71 .70 .73 .69 .74 .76 .73 .78 .74 .71 .68 .80 .72 .72 .70 .91 .97 .94 .93 .85 .108 .88 .95 .89 .108 .97 .91 .88 .92 .96 .92 .96 .92 .106 .108 .100 .98 .108 .101 .98 .95 .73 .76 .75 .78 .77 .82 .84 .80 .77 .83 .76 .76 .74 .78 .83 .83 .84 .83 .95 .93 .92 .88 .98 .90 .84 .82 .70 .67 .66 .69 .65 .74 .71 .73 .83 .76 .67 .64 .78 .81 .84 .80 .81 .87 .81 .80 .80 .80 .80 .84 .80 .76 .93 .93 .97 .94 .92 .104 .08 .108 .102 .110 .101 .04 .99 .102 .98 .100 .99 .97 .109 .108 .108 .102 .110 .110 .04 .99 .72 .78 .75 .76 .73 .80 .79 .74 .72 .80 .73 .72 .71 .89 .91 .90 .91 .87 .101 .101 .92 .92 .99 .96 .91 .89 .88 .91 .92 .91 .87 .101 .101 .92 .92 .99 .96 .91 .89 .88 .91 .92 .91 .87 .101 .101 .92 .92 .99 .96 .91 .89 .89 .70 .72 .72 .71 .76 .69 .66 .66 .73 .73 .64 .61 .75 .78 .78 .78 .78 .77 .81 .75 .74 .74 .81 .81 .74 .71 .35 .40 .40 .44 .44 .46 .41 .41 .45 .41 .39 .41														
.76 .81 .81 .81 .81 .84 .76 .75 .75 .82 .82 .76 .78 .70 .73 .76 .76 .74 .77 .69 .73 .71 .80 .74 .71 .70 .73 .69 .74 .76 .73 .78 .74 .71 .68 .80 .72 .72 .70 .91 .97 .94 .93 .85 1.08 .88 .95 .89 1.08 .97 .91 .88 .92 .96 .92 .106 .108 .100 .98 1.08 .101 .98 .95 .73 .76 .75 .78 .77 .82 .84 .80 .77 .83 .76 .74 .78 .83 .83 .84 .83 .95 .93 .92 .88 .98 .90 .84 .82 .70 .67 .66 .69 .65 .74 .71 .77 .73 .83 .76								1					The same	
70 73 76 76 74 77 49 73 71 80 74 71 70 173 49 74 76 73 78 74 71 68 80 72 72 70 191 97 94 93 85 108 98 95 89 108 97 91 88 92 96 92 106 108 100 98 108 101 98 95 73 76 75 78 77 82 84 80 77 83 76 74 74 78 83 83 84 83 95 93 92 88 98 90 84 82 70 .67 .66 .69 .65 .74 .71 .73 83 .76 .67 .64 78 81 .84 .80 .81 .87 81 .80 .80 .80 .80 .76 .69 93 <t< td=""><td>V</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td></t<>	V									-				
.73						1								
91 97 94 93 .85 1.08 98 95 89 1.08 97 91 88 92 96 92 1.06 1.08 1.00 98 1.08 1.01 98 95 .73 .76 .75 .78 .77 .82 .84 .80 .77 .83 .76 .74 .78 .83 .84 .83 .95 .93 .92 .88 .98 .90 .84 .82 .70 .67 .66 .69 .65 .74 .71 .77 .73 .83 .76 .64 .78 .81 .84 .80 .81 .87 .81 .80 .80 .80 .80 .80 .76 .78 .81 .84 .80 .81 .87 .81 .80 .80 .80 .80 .76 .93 .93 .97 .94 .92 .04 .95 .98 .96 .99 .101 .94 .99 .72														
92 96 92 96 92 1.06 1.08 1.00 98 1.08 1.01 98 95 1.73 76 75 78 .77 82 .84 80 .77 83 76 .76 .74 1.78 83 83 84 83 .95 93 92 88 98 90 84 82 1.70 .67 .66 .69 .65 .74 71 .77 .73 83 .76 .67 .64 1.78 81 .84 .80 .81 .87 81 .80 80 .80 .80 .84 80 .76 1.78 81 .84 .80 .81 .87 81 .80 80 .80 .84 80 .76 1.73 93 97 94 92 1.04 95 98 96 .99 1.01 .96 .89 1.02 98 1.00 .99 .97 1.09 1.08 1.02 1.10 1.10 1.04 .99 1.72 1.78 .75 .76 .73 .80 .79 .74 .72 80 .73 .72 .71 1.89 91 90 91 .87 1.01 1.01 .92 92 .99 96 .91 .89 1.88 91 .92 91 .87 1.01 .91 .92 .92 .99 .96 .91 .89 1.89 .70 .72 .72 .71 .76 .69 .66 .66 .73 .73 .64 .61 1.75 .78 .78 .78 .78 .77 .81 .75 .74 .74 .81 .81 .74 .71 1.35 .90 .90 .94 .94 .44 .44 .46 .41 .41 .45 .41 .39 .41														
.73 .76 .75 .78 .77 .82 .84 .80 .77 .83 .76 .76 .74 .78 .83 .83 .83 .84 .83 .95 .93 .92 .88 .98 .90 .84 .82 .70 .67 .66 .69 .65 .74 .71 .77 .73 .83 .76 .67 .64 .78 .81 .84 .80 .81 .87 .81 .80 .80 .80 .80 .84 .80 .76 .93 .93 .97 .94 .92 .04 .95 .98 .96 .99 1.01 .96 .89 .102 .98 .100 .99 .97 .109 .108 .108 .102 .110 .1.10 .104 .99 .72 .78 .75 .76 .73 .80 .79 .74 .72 .80 .73 .72 .71 .89 .91 .90 .91 .87 .101 .101 .92 .92 .99 .96 .91 .89 .88 .91 .92 .91 .87 .101 .91 .92 .92 .99 .96 .91 .89 .88 .91 .92 .91 .87 .101 .99 .97 .95 .101 .99 .94 .91 .69 .70 .72 .72 .71 .76 .69 .66 .66 .73 .73 .64 .61 .75 .78 .78 .78 .78 .78 .77 .81 .75 .74 .74 .81 .81 .74 .71 .35 .90 .90 .90 .94 .94 .94 .94 .94 .94 .94 .94 .94 .94					-									
.78 .83 .83 .84 .83 .95 .93 .92 .88 .98 .90 .84 .82 .70 .67 .66 .69 .65 .74 .71 .77 .73 .83 .76 .67 .64 .78 .81 .84 .80 .81 .87 .81 .80 .80 .80 .80 .80 .80 .80 .80 .80 .80										-				
.70 .67 .66 .69 .65 .74 .71 .77 .73 .83 .76 .67 .64 .78 .81 .84 .80 .81 .87 .81 .80 .80 .80 .84 .80 .76 .93 .93 .97 .94 .92 .04 .95 .98 .96 .99 1.01 .96 .89 1.02 .98 1.00 .99 .97 1.09 1.08 1.08 1.02 1.10 1.10 1.04 .99 .72 .78 .75 .76 .73 .80 .79 .74 .72 .80 .73 .72 .71 .89 .91 .90 .91 .87 1.01 1.01 .92 .92 .99 .96 .91 .89 .88 .91 .92 .91 .87 1.01 .91 .97 .95 1.01 .99 .94 .91 .69 .70 .72 .72 .71 .76 .69 .66 .66 .73 .73 .64 .61 .75 .78 .78 .78 .78 .77 .81 .75 .74 .74 .81 .81 .74 .71 .35 .90 .90 .94 .94 .94 .94 .94 .94 .91 .95 .41 .99 .91														.74
.78 .81 .84 .80 .81 .87 .81 .80 .80 .80 .84 .80 .76 .93 .93 .97 .94 .92 .04 .95 .98 .96 .99 1.01 .96 .89 1.02 .98 .00 .99 .97 .09 .08 .08 .02 .10 1.10 .04 .99 .72 .78 .75 .76 .73 .80 .79 .74 .72 .80 .73 .72 .71 .89 .91 .90 .91 .87 1.01 1.01 .92 .92 .99 .96 .91 .89 .88 .91 .92 .91 .87 1.01 .91 .92 .92 .99 .96 .91 .89 .88 .91 .92 .91 .87 1.01 .99 .97 .95 .101 .99 .94 .91 .69 .70 .72 .72 .71 .76 .69 .66 .66 .73 .73 .64 .61 .75 .78 .78 .78 .78 .77 .81 .75 .74 .74 .81 .81 .74 .71 .35 .90 .90 .94 .94 .94 .94 .94 .94 .91						.83							84	82
93 93 97 94 92 1.04 95 98 96 99 1.01 96 89 1.02 98 1.00 99 97 1.09 1.08 1.08 1.02 1.10 1.10 1.04 99 72 1.09 1.08 1.08 1.08 1.02 1.10 1.10 1.04 99 72 1.78 75 76 73 80 79 74 72 80 73 72 71 89 91 90 91 87 1.01 1.01 92 92 99 96 91 89 88 91 92 91 87 1.01 99 97 95 1.01 99 94 91 69 70 72 72 71 76 69 66 66 73 73 64 61 75 78 78 78 78 77 81 75 74 74 81 81 74 71 35 90 90 94 94 94 94 94 96 91 97 97 97 98 78 78 78 78 78 78 78 78 78 78 78 78 78		.70	.67	.66	.69	.65	.74	.71	.77	.73	.83	.76	.67	,64
1.02 98 1.00 99 97 1.09 1.08 1.02 1.10 1.10 1.04 99 7.2 78 .75 .76 .73 .80 .79 .74 .72 .80 .73 .72 .71 .89 .91 .90 .91 .87 1.01 1.01 .92 .92 .99 .96 .91 .89 .88 .91 .92 .91 .87 1.01 .99 .97 .95 1.01 .99 .94 .91 .69 .70 .72 .72 .71 .76 .69 .66 .66 .73 .73 .64 .61 .75 .78 .78 .78 .78 .77 .81 .75 .74 .74 .81 .81 .74 .71 .35 .90 .90 .94 .94 .94 .94 .94 .91 .95 .41 .95 .41 .39 .91		.78	81	.84	.80	.81	.87	81	.80	80	.80	24	.80	.76
1.02 98 1.00 99 97 1.09 1.08 1.02 1.10 1.10 1.04 99 7.2 78 .75 .76 .73 .80 .79 .74 .72 .80 .73 .72 .71 .89 .91 .90 .91 .87 1.01 1.01 .92 .92 .99 .96 .91 .89 .88 .91 .92 .91 .87 1.01 .99 .97 .95 1.01 .99 .94 .91 .69 .70 .72 .72 .71 .76 .69 .66 .66 .73 .73 .64 .61 .75 .78 .78 .78 .78 .77 .81 .75 .74 .74 .81 .81 .74 .71 .35 .90 .90 .94 .94 .94 .94 .94 .91 .95 .41 .95 .41 .39 .91		93	93	97	94	92	1.04	95	.98	96	.99	1.01	.96	.89
72 78 .75 .76 .73 .80 .79 .74 .72 80 .73 .72 .71 .89 .91 .90 .91 .87 1.01 1.01 .92 .92 .99 .96 .91 .89 .88 .91 .92 .91 .87 1.01 .99 .97 .95 1.01 .99 .94 .91 .69 .70 .72 .72 .71 .76 .69 .66 .66 .73 .73 .64 .61 .75 .78 .78 .78 .77 .81 .75 .74 .74 .81 .81 .74 .71 .35 .90 .90 .94 .94 .94 .94 .94 .94 .91 .95 .91 .99 .91		1.02	.98	1.00	.99	.97	1.09	1.08	1.08	1.02	1.10	1.10	1.04	99
.89 91 90 91 87 1.01 1.01 92 92 99 96 91 89 .88 91 92 91 87 1.01 99 97 95 1.01 99 94 91 .69 7.0 7.2 7.2 7.1 7.6 69 66 66 7.3 7.3 64 61 .75 7.8 78 78 78 77 .81 75 74 74 .81 .81 .74 .71 .35 40 40 44 44 44 46 41 41 45 41 39 41														
.88 91 92 91 87 1.01 99 97 95 1.01 99 94 91 .69 70 72 72 71 76 69 66 66 73 73 64 61 .75 78 78 78 77 .81 75 74 74 .81 .81 .74 .71 .35 40 40 44 44 46 41 41 45 41 39 41														
.69 70 72 72 71 76 69 66 66 73 73 64 61 .75 78 78 78 77 .81 .75 74 74 .81 .81 .74 .71 .35 40 40 44 44 46 41 41 45 41 39 41	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1													
.75 .78 .78 .78 .77 .81 .75 .74 .74 .81 .81 .74 .71 .35 .40 .40 .44 .44 .46 .41 .41 .45 .41 .39 .41								-						
35 40 40 44 44 46 41 41 45 41 39 41														
100 .66 .66 .66 .66 .66 .66 .66 .66										0.00				
		.00	6/	.06	.00	13	10	.60	190	.00	./0	169	.00	.66

1	D 42 - 1	Tool 1/	Flicks Ma			5 /					5-2		
XI	P-42 airplone	Test No Run No.	riight No.	1	2	5-/	4	5	1		5-2	4	5
inl	port-nose low- let-velocity wling	Atm. press Ambient Air o, density	oress., in. H _e O cure, in. H g . Temp., °F ratio	36.5 7.17 .646	35.5 /6.46 -2 .624	34.4 5.8 -5 .603	333 5 8 -9 .584	32,3 4.54 -/2 .563	.640	35,1 6.42 0 620	34.3 15.82 -5 .603	332 5./3 -8 .58/	31.6 4.5 -10 .560
		Density A		14450	15250			18350	14500	15450	16300	17400	18500
		Rpm. Bhp.				863	840	811	914				
		Manifold pr	ess., in. Hg.	40.3	38.9		36.3 Cufi		40.4			36.4	34.9
				*					506	no t	911		~ ~
		Į·		-					5Ura		atio	<i>D</i> /	
F	naina Prasaura Tuta	1/ 07		.30	.31	.30		.31	31			.30	
2	ngine Pressure Tube Locations	1-R 3-R		.30	.30	.30	.31	.29	.30	.30	.31	.29	.30
		4-R 6-R	sheltered tubes		.29	.28	.30	.28		.30 .32		.28	.29
	cyl. ~	7-R	behind	.32	.32	.32	.32	.32	.32	.32	.32	.31	.32
	30	10-R	engine	.33	.34	.34	.34	.33	.34	.34	.34		.34
		12-R		.31	132	.32	.32	.31	.32		.32		.32
	4 12	14-R) 1-EB		.81	.82	.80	.82	.80	.82	.82	.82.	.81	.30
	5 1	3-EB		.70	.69	.70	.69	.70		.70	.70	.69	.69
		4-EB 6-EB	exhaust	.80	.81	.80	.80	.80	.81	.80		.80	.80
	910	7-EB	side of	.80	.80	.79	.80	.79	.81	.80		.80	.80
	7 6	10-EB	barrel	.80	.82	.80	.81	.80	.81	.8 2	.82	.80	.82
		12-EB		1	,75		.75	.75	.76	.77	.76 .84	.75	.75
	Cylinder no. 1	14-EB)	.81	.81	.81	.81	.80	.83	.83	.82	18.	.82
	I-TH A	3-EH 4-EH		.75	.73	.73	.74	.73	.74	.75	.74	.74	.74
30	1-XH	6-EH	exhaust	.75	.75	.74	.74	.73	.75	.75	.75	.73	.74
ocations	OF FEH	7-EH 9-EH	side of	.83	.83	.82	.83	,76		.77	.77	.76	.85
100	0. 0	10-EH	1	.81	.81	.80	.81	.80	.82	.83	.82	.82	.82
0 6	1-18	12-EH 14-EH				.80					.82		
ing tube	1-28	1-TH		.82	.83	.82	.83	.81	.83	.83	.84	.82	.83
2.	0- I-R	3-TH 4-TH		.72	.72	.71	.72	.72	.73	.73	.73	.72	.72
in 9		6-TH	top of	.72	.72	.71	.72	.70		.71	.71	.70	.71
designating typical cyli	Cylinder no. 3	7-TH	head	.80	.80	.80	.82	08.	.80	.81	.81	,80	08.
design	3-774-40	10-TH 12-TH	*	.74	.74	.74	.75	.74	.74	.75	.75	.74	.74
	3-EH2-10	14-TH		.72	.74	.74	.73	.73	.74	.75	.75	.74	.75
60	3-EH	1 - IH 6 - IH	intake side of	.79	.81	.80	.82	.83	.80	.81	.81	.80	.80
200		10-IH)	head	.87	.89	.89	.89	.88	.87	.89 -	.88	.87	.87
Method of For	3-EB-	1- IB 6- IB	intake side of	.77	.78	.76	.77	.76	.78	.78	,78 ,83	.77	.77
2	3-£82->0	10-IB)	barrel	.79	.81	.81	,80	.80	.81	.82	.81	.80	.80
		3 - EH2 4 - EH2		.75	.75	.74	.75	.75	.75	.76	.75	.74	.75
	0 <u>←</u> 3-R	3 - EB	2	,60	.59	.60	.60	.60	.60	.60		.60	.60
,		14 - EBZ		.65	.64	.65	.65	.64	.66	.64	.04	.64	.64

Ind. cirspeed, mph.		7	- 1 - 10						,					-
Ind. cirspeed, mph Ressure altitude Fressure altales Fressure altales Fressure altales Fressure Fressure altales Fressure Fressure Fressu		1			4	+				5	,			4
9c Pressure altitude range, ft. Av. free air temp, ft. Av. free air temp, ft. Av. free air temp, ft. Av. manifold press. Rpm Av. manifold press. Av. manifold press. Rpm Av. manifold press. Rpm Av. manifold press. Av	Ind win d	100												
Fressure attrible range, fri Av. the property temp, from the first and produce and produc	_										1			
Av. Eng. 18 119 12 12 12 12 12 12 12 12 12 12 12 12 12	Pressure altitude range, ft.	4000	11100	15000	- NEED	2400	- 8400	1230	16/00	19700	5100-	/32.00	-/630D	- 1950
Av. manifold press. #46 407 357 301 398 402 386 338 366 430 369 330 28. #25 50	Av. free-air temp, F										00202			-7
### ### ##############################														
Pressure catio, Pige -28 -28 -27 -28 -33 -32 -33 -33 -33 -35 -36 -36 -33 -37 -37 -37 -37 -37 -37 -37 -37 -37														- / /
Pressure tratio, Fige -28 -28 -27 -28 -23 -32 -32 -32 -33 -35 -36 -36 -33 -37 -37 -37 -37 -37 -37 -37 -31 -31 -31 -32 -32 -33 -34 -36 -33 -33 -34 -36 -33 -33 -34 -36 -33 -33 -34 -36 -33 -33 -34 -36 -33 -31 -31 -31 -31 -31 -31 -31 -31 -31		AUN	o. ric								FUR	l me	b, chi	b
-28 -28 -27 -28 -23 -32 -33 -33 -33 -35 -36 -36 -33 -37 -27 -27 -27 -25 -27 -31 -31 -31 -32 -30 -33 -33 -35 -36 -36 -33 -31 -31 -31 -31 -31 -31 -31 -32 -30 -33 -33 -35 -36 -36 -33 -31 -31 -31 -31 -31 -31 -31 -31 -31		-		_ (-				-				
-27 -27 -25 -27 31 -31 -31 -30 -39 -33 -34 -36 -36 -31 -31 -31 -31 -35 -35 -35 -35 -34 -38 -37 -38 -41 -37 -31 -31 -31 -35 -35 -35 -35 -34 -38 -37 -38 -44 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34 -34									_					
131 131 131 135 135 135 134 138 137 138 141 134 144														
-14 -14 -14 -16 -20 -17 -16 -19 -21 -21 -22 -24 -24 -24 -25 -17 -16 -17 -16 -16 -24 -17 -20 -21 -21 -22 -23 -24 -24 -26 -26 -24 -26 -2											1			
-18 -17 -16 -16									7.					
-18 -18 -18 -18 -24 -23 -23 -23 -23 -23 -25 -26 -26 -26 -27 -27 -23 -23 -27 -27 -23 -23 -23 -23 -23 -25 -26 -26 -26 -26 -26 -26 -26 -26 -26 -26														
-28 -28 -27 -27 -33 -33 -33 -33 -35 -36 -36 -36 -36 -36 -36 -36 -36 -36 -36		-18	-18	-18	-18	-24	-23	-95	-,23	-93	-53	-56	-26	7 :
\$2														
70		.82	.80	.80	.77	.82	.63	.76	.79	.77	.86	.78	85.	17.
91											100			
94 94 91 91 1.04 1.04 1.04 1.05 1.05 1.00 1.00 1.00 1.05														
97 97 94 93 102 98 94 96 105 96 96 34 36 36 36 38 37 98 90 94 90 105 96 90 38 36 38 38 39 30 34 79 79 34 34 35 38 37 77 77 77 77 77 77		1											*	
86 84 84 79 89 89 90 84 79 79 84 82 82 83 77 77 77 77 73 80 77 80 75 73 82 74 73 75 70 67 65 61 71 69 67 61 70 64 62 63 83 81 79 73 74 84 80 77 74 82 78 74 77 74 82 78 74 77 74 82 78 74 77 74 82 78 76 73 74 77 74 77 74 82 78 76 73 74 77 74 77 74 77														
79 77 77 72 30 79 80 75 72 82 74 72 75 70 67 65 61 71 69 69 67 61 70 64 62 63 63 81 79 73 89 84 80 77 74 88 78 74 77 75 73 72 70 69 84 78 74 77 74 88 78 74 74 75 73 72 70 69 84 78 74 77 74 82 78 76 73 74 75 73 72 70 69 84 78 74 77 74 82 78 76 73 74 75 74 75 74 75 75 75 76 71 68 87 84 80 80 80 76 84 80 80 80 80 80 80 76 84 80 80 80 80 80 80 80 80 80 80 80 80 80		1												
70 .67 .65 .61 .71 .69 .69 .67 .61 .70 .64 .62 .62 .83 .81 .79 .73 .89 .84 .80 .77 .74 .88 .78 .74 .75 .73 .72 .70 .69 .84 .75 .74 .77 .74 .82 .78 .76 .73 .72 .70 .69 .84 .75 .74 .77 .74 .82 .78 .76 .73 .94 .93 .91 .87 .80 .80 .80 .80 .80 .80 .80 .80 .80 .80			_	_	-									-
73 72 70 69 84 78 74 77 74 82 78 76 73 94 93 91 87 87 87 87 88 88 89 82 91 87 95 87 87 87 87 88 100 100 100 100 100 100 100 100 100		.70	.67	.65	.61	.71	.69	.69	.67	.61	.70	.64	.62	.63
.94 .93 .91 .87 1.09 1.02 .98 .96 1.05 1.00 .96 .96 .85 .87 .87 .88 .89 .82 .91 .87 .87 .87 .87 .88 .90 .90 .90 .106 1.02 1.16 1.06 1.04 1.09 1.09 1.09 1.09 1.09 1.00 1.00 1.11 1.06 1.04 1.00 1.11 1.06 1.04 1.00 <t< td=""><td></td><td></td><td>-</td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></t<>			-											
1.06 1.00 .91 .94 1.13 1.10 1.08 1.06 1.02 1.16 1.06 1.04 1.06 1.03 1.00 .94 1.19 1.16 1.17 1.12 1.06 1.19 1.09 1.09 1.09 1.06 .85 .87 .84 .80 .90 .90 .91 .85 .85 .85 .85 .85 .86 .80 .80 .76 .73 .81 .83 .79 .79 .76 .85 .75 .73 .76 .71 .68 .81 .79 .75 .74 .73 .81 .75 .71 .73 .75 .71 .69 .83 .80 .74 .76 .73 .81 .75 .71 .73 .75 .71 .69 .83 .80 .74 .76 .73 .81 .75 .71 .73 .73 .75 .71 .69 .83 .80 .74 .76 .73 .81 .77 .73 .73 .75 .71 .69 .83 .80 .74 .76 .73 .81 .77 .73 .73 .75 .71 .69 .83 .80 .74 .76 .73 .81 .77 .73 .73 .74 .74 .74 .75 .76 .71 .84 .84 .84 .84 .87 .93 .90 .95 .88 .86 .94 .88 .88 .91 .67 .70 .68 .65 .75 .75 .74 .74 .71 .79 .70 .67 .71 .80 .83 .80 .78 .78 .80 .78 .78 .78 .78 .78 .78 .78 .78 .78 .78							1.02	.96						
1.06 1.03 1.00 .94														
.84 .84 .80 .76 .84 .83 .81 .78 .85 .77 .78 .80 .80 .76 .73 .81 .81 .77 .70 .71 .82 .73 .73 .73 .71 .68 .81 .77 .73 .81 .73 .71 .73 .73 .71 .68 .80 .74 .														
\$0		1												
75 76 71 68 81 77 75 74 73 81 75 71 73 73 75 77 16 73 75 71 68 81 77 75 77 75 77 75 77 16 75 77 17 75 73 73 73 75 77 16 75 77 17 76 75 76 77 17 76 77 17 76 77 17 76 77 17 76 77 17 76 77 17 17 106 107 107 107 107 107 107 107 107 107 107		1												
1.00 .98 .94 .89 1.15 1.06 1.00 1.04 1.02 1.06 1.04 1.01 .98 .98 .97 .97 .91 1.06 1.08 .97 1.05 1.03 1.10 1.02 1.02 1.02 1.03 .77 .77 .79 .74 .84 .92 .83 .81 .79 .86 .78 .78 .88 .84 .84 .84 .79 .93 .90 .95 .88 .86 .94 .88 .88 .91 .67 .70 .68 .65 .75 .75 .74 .74 .71 .79 .70 .67 .71 .80 .82 .79 .76 .84 .86 .82 .81 .79 .88 .80 .78 .81 .79 .88 .80 .78 .81 .79 .88 .80 .78 .81 .79 .88 .80 .78 .81 .95 .98 .95 .98 .95 .98 .133 1.10 1.05 1.05 1.05 1.05 1.05 1.05 1.05		.75	.76	.71	.68	.81	.79	.75	.74	.73	.81	.75	15.	.73
98 97 97 91 1.06 1.08 97 1.05 1.03 1.10 1.02 1.02 1.02 1.02 1.02 1.02 1.03 1.07 77 77 79 74 84 92 83 81 79 86 78 78 88 91 84 84 84 84 79 93 90 95 88 86 94 88 88 91 67 70 68 65 75 75 74 74 71 79 70 67 71 80 82 78 81 91 79 88 80 78 81 95 98 95 89 1.06 1.07 1.02 1.03 1.07 1.02 1.00 1.11 1.05 1.02 1.08 98 1.13 1.10 1.05 1.05 1.05 1.05 1.05 1.05 1.05														
.84 .84 .84 .79 .93 .90 .95 .88 .86 .94 .88 .89 .91 .67 .70 .68 .65 .75 .75 .74 .74 .71 .79 .70 .67 .71 .80 .82 .79 .76 .84 .86 .82 .81 .79 .78 .80 .78 .81 .79 .88 .80 .78 .81 .79 .88 .80 .78 .81 .95 .98 .95 .99 .106 1.07 1.02 1.03 1.07 1.02 1.00 1.01 1.05 1.05 1.05 1.05 1.05 1.05														
.67 .70 .68 .65 .75 .75 .74 .74 .71 .79 .70 .67 .71 .80 .82 .79 .76 .84 .86 .82 .81 .79 .88 .80 .78 .81 .95 .98 .95 .89 1.06 1.07 1.02 1.03 1.07 1.02 1.00 1.11 1.05 1.02 1.08 .98 1.13 1.10 1.05 1.05 1.05 1.05 1.08 1.05 1.05 1.05 1.05 1.05 1.05 1.05 1.05														
1.80														
1.05 1.02 1.08 .98 1.13 1.10 1.05 1.05 1.05 1.05 1.05 1.05 1.05		.80	.82	.79	.76	.84	.86	.82	.81	.79	8.8.	.80	.78	.81
78 75 75 73 80 78 74 77 74 81 74 75 75 75 77 74 81 74 74 75 75 75 75 75 75 75 75 75 75 75 75 75														
98 94 94 94 91 99 100 101 98 102 195 95 98 31 73 07 25 24 17 17 67 17 23 83 07 87 75 76 17 17 17 17 17 17 17 17 17 17 17 17 17		.78	.75	.75	.73	.80	.78	.72	.77	.7.4	.81	.74	.74	.75
78 .70 .68 .65 .71 .73 .71 .65 .75 .70 .67 .66 .71 .73 .87 .75 .75 .76 .77 .78 .81 .67 .77 .78 .78 .78 .78 .78 .78 .78 .78 .7														
cr. sr. 8r. 48, sr. cr. 8r. 08, r8, 8d. cr. dr. 7r.							-		-	_		-	-	-
		.77	.76	.73	.68	.87	.80	.78	.73	.72	,84	.78	.72	.73
41. 41. 44. 44. 45. 45. 64. 64. 44. 45. 44. 45. 44. 45. 46. 46. 46. 46. 46. 47. 46. 46. 46. 46. 46. 46. 46. 46. 46. 46		110000000000000000000000000000000000000											-	

	Table I(b) PRESSURE DATA
XP-42 Airplane Test No Flight No.	8-22 1 2 3 4 5 1 2 3 4 5
Short-nose low- inlet-velocity cowling With Ear, without cuffs Which Ear, without cuffs Manifold Press, in the control of the control of the cuffs Ambient Air Temp, For density ratio Density Altitude, for the cuffs Manifold Press, in the cuffs True Airspeed, moth. Atm. pressure, in the cuffs of density ratio Density Altitude, for the cuffs Manifold Press, in the cuffs of the cuff	17.10 16.50 15.79 15.16 14.56 17.22 16.56 15.91 15.23 14.66 4 -2 -3 -7 -9 9 7 1 -2 -8 6.39 6.24 .599 .580 .560 6.636 .614 .598 .576 .561 1450 15.20 16.50 17.50 1845 16.630 17.50 1845 16.630 17.50 1845 17.50 1845 17.50 1845 17.50 1845 17.50 1845 17.50 1845 17.50 1845 17.50 1845 17.50 1845 17.50 1845 17.50 1845 17.50 1845 17.50 1845 17.50 1845 184
	Pressure ratio, Plac
A-TPS A-	75 76 76 76 76 77 77 77 77 76 76 76 77 76 76
Location of Pressure Tubes in Annulus A-LS1 3 trapes Tinges in Annulus A-LS1 3 trapes A-LS1 4 trapes A-LS1 4 trapes A-LS1 4 trapes A-LS1 5	\ \begin{array}{c ccccccccccccccccccccccccccccccccccc
OFFSI O-FPI	84 84 84 84 85 85 85 84 83 84 85 85 86 85 85 85 86 85 85 85 86 86 87 87 86 87 86 87 86 662 62 61 62 62 62 61 61 60 61 62 660 61 59 60 60 59 59 59 58 59 59
Carburetar Scoop Copy of Copy	98 98 98 98 98 98 98 98 97 97 98 98 98 98 98 98 98 98 98 97 97 97 80 80 80 80 79 79 79 78 79 79 77 78 77 77 76 77 76 77 76
C-H of S C-3/ Flush static C-TH Impact press	

74016	,		21/11/							
Marin Carlo	Harrier,		9-21	/				9.	-20	-
	1	2	3	4	5	/	2	9	4	5
	-	2		7		-	2		7	
Ind. airspeed, mph.	158	157	155	154	153	138	138	138	136	137
	12.4	12.2	11.9	11.8	11.7	9.5	9.4	9.4	9.2	9.3
Pressure altitude ?			12300	16300	19000	2500-	8400-	13100-	17/00-	/9700-
range, ft.	6400	8800	13300	17200	20000	3900	9500	14100	17800	20900
									_	10
Av. free air temp, 4	25	24	12	-/	-//	3/	25	10	-5	-10
Av. bhp.	890	890	875	775	695	960	930	800	675	600
Av. manifold press.	40.0	40.0	38.7	33.6	30.0	427	41.6	364	31.7	28.8
Rpm.	-	2	540			-	-2	525		-
										- 4
	AUI	60 R	ich,	clim	6	FUL	PIC	h, 01	imb	
	1							c- ·		
	_	WIII	h fa	ris H	inne	041	CUIT	3		
			-							
Pressur	e -	2+10	P6.	m.						
7 7 60207		.,,,,	17	,						
	80	.78	.82	.82	.81	.81	.87	.80	.80	.78
	.92	.91	.90		.85	95	96	.88	.87	.83
				.89						
	1.03	1.02	.98	.95	92	1.10	1.03	98	. 94	
	96	.94	97	.97	.96	1.08	1.05	1.00	.95	94
	.87	.87	.84	.88	.87	94	92	.85	.85	.83
	.70	.71	72	.72	.72	.65	.74	.66	.67	69
	.72	.74	.72		.72	.68	.73	.69	.66	67
	150			.72						
	.7/	.7/	.73	.73	.79	.7/	.73	.70	.7/	.68
	87	,83	.88	85	.85	94	.98	91	.87	.86
	1.02	1.04	.97	93	.93	1.15	1.16	100	.99	.98
	1.19	1.18	1.08	1.04	1.04	1.32	1.25	112	106	105
	1.04	1.01	1.03	1.01	1.01	1.14	1.14	104		.97
	97	96	98	.92	.92	1.05	94	94	94	92
	.81	.78	.78	.79	.79	.7/	18.	.76	.77	.74
	.83	.80	.81	.82	.81	.84	.87	.81	.79	72
	.83	82	.82	.81	.81	.86	.86	80	.80	.80
	65	.69	.75	.81	.80	.67	.65	71	71	73
					- 10					
	90	90	.94	.93	93	.94	92	.86	90	.90
	1.08	1.00	1.01	1.03	1.02	1.09	1.05	1.04	100	198
	.98	1.03	1.03	1.04	1.03	1.07	1.03	1.03	.98	.98
	82	.82	86	85	85	.84	.82	.76	.79	.79
	.90	.89	.88	87	87	.96	.89	.85	.86	.82
	.91	.88	.92	88	.90	.96	.96	90	.88	.86
	.97	.92	.90	.91	.88	.99	.97	.94	.89	87
	.75	.78	.80	.84	.85	.66	72	74	.77	.76
	.78	.85	.87	91	.89	.72	.74	.79	.79	.79
	.82	.85		92	.93	.76	80	.80	84	.85
						,			.65	
	.68	.68	.7/	.72	.73	-58	.63			
	68	.66	.69	.73	.73	.55	.61		.65	
	.65	,66	.70	.74	.73	.60	.64	.65	.69	.67
	28	28	31	.32	33	.18	.23	23	.25	25
	.22	24	.23	.26	.28	.14	.21	./7	21	23
	~~	,								
		0.		-						
	.19	.20	ADDRESS OF THE PERSON	24	24	./2	No. of Persons	AC ALL DESCRIPTION OF	.20	.2/
	.87	.85	23	.90	90	.84	.83	.82	.86	.85
	.90	.85	.87	91	.93	.86	88	.86	.87	.88
	87	.90	90	.93	96	.90	91	91	.89	91
	.90	.91	92	.95	96	.90	90	.87	92	93
		.89	.94	.93	.97	.89	.89	.85	.89	.96
	.57	51	.48	.57	.61	.40	.32	.33	.42	46
	.50	45	43	.48	.56	.37	.21	.23	.35	42
	.48	.42	37	44	53	33	.16	.23		.37
	.47	45	37	.44	52	.32	./7	.20	.33	.37
	.56	49	41	.53	.57	.34	.25	.30	.35	.42
	-									

Table I(b) (continued)

	lable 1(b) (continu	00/									
XP-42 Airplane	Test No Flight No.			11-1	_	_	,		11-2 3	1	5
SHOTT-NOSE low-	Run No.	/	2	3	4_	5		2	<u> </u>	4	ر ت
inlet-velocity	Trus airspeed, mph.					33/			328		ALL THE STATE OF T
cowling	qc, impact press, in. H.O					31.3			32.0		
	Atm. pressure in. Mg. Ambient air temp, F	15	16.10	15.84	13.10	14.5A -2	2	13.01	-4		-10
No fan, no cuffs	o, density ratio	.628	.614	.590	57/	.552	.618	.594	,577	.555	.538
	Density altitude, ft.	15050			17950	18950	15500			18800	20000
	Rpm Bhp	871	26		8 in	794	860		803	780	752
	Manifold press, in Hg					339			35.1		
*	, , ,	1	igh	50	ee4	1	h	igh	5	086	d
			_						-		
		Pr	e554	ire	rat	io, p	190				
,	A-TPI)	.72	.7/	.7/	.71	.72	.73	.72	.72	.72	.7/
- 7		.74	.73	.74	.74	.73	74	.74	.73	.74	.75
A-TP5 A-TS3_ A-TP4	2 seam Top	90	.85	.85	.84	.84	90	85 90	.84	.84	.84
A-TS2 A-TP3	5 rake	.88	.86	.86	-86	.84	.86	.88	.86	. 86	-86
A-TSI A-TP	6 0	.68	.68	.68	.68	.68	.68	.68	.68	.68	.68
\$ 2	2 3 2 2 3 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	.68	.68	.68	.68	.68	70	.70	.70	.70	.7/
34.4	A-RPI	.22	.71	71	.7/	.72	.72	.7/	.72	.7/	.7/
A-RPI J. A-	P5 2 138	74	.73 .78	.73 .79	.73	.74	.73	.72	.72	.72	.72
A-RSI A-L	13 A Right	29	.87	.88	.87	.88	.88	.87	.87	.88	.87
**0.	5) Survey	.84	.84	.83	.83	.84	.83	.83	.83	.84	.82
	A-R51	-	.69	.68	.70	.69	.69	.70	.69	.70 .71	.69
Location of pressure	Shaffe	.70	.72	.72	.73	.72	.73	.72	.73	.72	.73
tubes in annulus	A-LPI)	7.4	.73	.74	.74	.73	.74	74	.74	.74	.74
	2 3 68 105	73	.74	.73	.73	.73	.75	.75	.74	.74	.75
	1 89 401	.84	.84	.83	.83	.84	.84	. 86	.84	-86	.83
	5) 30110	.78	.79	.78	.78	.78	80	.80	.79	.80	.80
	A-721	7/	.71	.70	.70	70	.7/	.7/	.7/	.72	.71
	2) to	.72	.73	.72	.72	72	.73	.73	.73	.74	.73
Oil cooler pressure tube loc	cations O-FPI	.91	.92	.92	.91	-91	.92	.92	,92	.91	.92
0-F51 0-FPI 0-	RPI 3	.96	.96	.96	.97	.95	.97	.97	.97	.96	.96
0-F52 0-FP2	200 0 501)	.85	.84	.85	.25	.84	.85		.84	.85	.84
Xo-FPS	0-F3/ 3urvey	.86	.86	.85	.85 .86	.85	.86	,86	.87	.86	.85
	2 200)	101	.62		.62		,63	.63	.62	.63	. 62
0-F53	2 Rear	.59	.58	.58	,59	.58	.59	.58	.59	.60	,58
shielde impact t	ube 0-SP Survey	56	.56	.56	,55	.55	.57	,56	.56	. 56	.56
Carburetor presure		.94	.94	.94	.93	.94	.95	.94	.94	.94	.93
Timbe locations	2 Impact	.96	.96	,95	.94	.95	.95	.96	95	,94	.94
	3 tubes	.97	.96	.96	.97	.95	.96	.97	.97	.96	.95
b C-P5	5/	98	:97	.97	.97	.97	.97	.98	.96	.96	.96
C-P5 00 00 00 C-S40	C-51	.80	.80	.79	.79	.80	.79	.81	.79	.77	.79
C-P3 0 - 0 C-53	3 Static tubes	.77	.77	.76	.78 .7 6	.75	.75	.76	.76	.76	.75
C-P2 0 - 52 tes	4	75	.75		.75	.74	.75	.75	.76	.76	.75
	5)	-									
4.03" C-SI	c -TH Impact press. in carb three	72	,73	73	.72	.73	.72	.73	.73	.73	.73
	press. In cara Inrea	1"-	.,-								

Table Ib) (continued)

10-2	14151	_	(-)	1000		-				
Ind. airspeed, mph. Q Pressure Ultitude Tange, ft. Av. free oir temp, °F Av. bhp. Av. Thanifold press. Pressure ratio, p/q Ind. airspeed, mph. Ind. airspeed, mph. Av. free oir temp, °F Av. bhp. Av. Manifold press. Rpm Ind. airspeed, mph. Ind. airspeed, mph. Av. free oir temp, °F Av. bhp. Av. Manifold press. Rpm Ind. airspeed, mph. Ind. airspeed, mph. Av. free oir temp, °F Av. bhp. Av. Manifold press. Rpm Ind. airspeed, mph. Ind. airspeed, mph. Av. free oir temp, °F Av. bhp. Av. Manifold press. Rpm Ind. airspeed, mph. Ind. airspeed, mph. Av. free oir temp, °F Av. bhp. Av. Manifold press. Rpm Ind. airspeed, mph. Ind. airspeed, mph. Av. free oir temp, °F Av. bhp. Av. Manifold press. Rpm Ind. airspeed, mph. Ind. airspeed, m		/			4	1			4	5
Tressure dititude france, it. Some space was also been lead 1500 and 1500 lead 1500 le	Ind airsneed mah	156				139	141			
Exessive altitude range, 14. Av. free air temp, 9	,									
Av. free oir temp, 95 Av. bhp. Av. Manifold press. Rpm	Bressure altitude?					The same of the sa				
Av. Manifold press. 900 920 820 720 920 890 785 780 600 39.7 39.8 349 305	range, tt.)									
Av. Monifold press. 397 398 349 305										
Rpm	Av. Manifold press.									
Pressure ratio, p/qc		-				-				-
Pressure ratio, p/q _c .74 .71 .70 .79 .77 .12 .44 .68 .72 .75 .73 .73 .81 .84 .80 .83 .82 .80 .72 .77 .72 .74 .75 .73 .73 .85 .85 .87 .80 .89 .80 .78 .77 .72 .74 .75 .73 .73 .85 .87 .80 .89 .80 .78 .77 .72 .74 .85 .85 .87 .80 .89 .87 .80 .83 .84 .84 .84 .84 .84 .84 .84 .84 .84 .84		2.4		6 0/10	m.h	E.A	-	6 -1	in A	
Pressure ratio, P/qc 1.74		7010		No f	nn .	nn c	iffs	5		-
. 74 . 7/ . 7/ . 70 . 79 . 77 . 72 . 49 . 68 . 72 . 76 . 72 . 70 . 78 . 74 . 75 . 73 . 73 . 8/ . 84 . 80 . 83 . 82 . 80 . 78 . 77 . 72 . 93 . 87 . 80 . 87 . 93 . 90 . 93 . 84 . 24 . 93 . 90 . 98 . 93 . 90 . 93 . 84 . 24 . 66/ . 67 . 67 . 67 . 67 . 67 . 62 . 63 . 69 . 67 . 64 . 68 . 68 . 68 . 62 . 63 . 69 . 67 . 64 . 68 . 68 . 68 . 62 . 64 . 68 . 64 . 65 . 70 . 67 . 67 . 62 . 63 . 7/ . 70 . 69 . 67 . 75 . 7/ . 71 . 71 . 67 . 65 . 69 . 78 . 74 . 75 . 8/ . 74 . 75 . 72 . 71 . 82 . 86 . 83 . 83 . 84 . 82 . 91 . 72 . 73 . 81 . 94 . 90 . 90 . 90 . 90 . 91 . 94 . 90 . 90 . 90 . 90 . 91 . 94 . 90 . 90 . 90 . 91 . 94 . 90 . 90 . 90 . 91 . 94 . 90 . 90 . 90 . 91 . 94 . 90 . 90 . 90 . 91 . 94 . 90 . 90 . 90 . 91 . 94 . 90 . 90 . 90 . 94 . 94 . 92 . 95 . 87 . 82 . 84 . 85 . 86 . 85 . 87 . 87 . 10 . 70 . 68 . 10 . 12 . 64 . 63 . 63 . 69 . 64 . 66 . 68 . 68 . 68 . 68 . 68 . 67 . 14 . 70 . 70 . 68 . 10 . 12 . 64 . 63 . 63 . 69 . 64 . 64 . 65 . 88 . 87 . 87 . 10 . 70 . 70 . 70 . 74 . 73 . 73 . 68 . 71 . 73 . 74 . 70 . 70 . 74 . 73 . 73 . 68 . 71 . 73 . 74 . 70 . 70 . 74 . 73 . 73 . 68 . 71 . 73 . 74 . 70 . 70 . 74 . 73 . 73 . 68 . 71 . 74 . 75 . 76 . 77 . 78 . 77 . 78 . 77 . 78 . 87 . 86 . 88 . 83 . 85 . 88 . 92 . 87 . 87 . 86 . 88 . 83 . 85 . 88 . 92 . 87 . 87 . 86 . 88 . 83 . 85 . 88 . 92 . 87 . 87 . 86 . 88 . 83 . 85 . 88 . 92 . 87 . 77 . 87 . 77 . 78 . 76 . 71 . 72 . 71 . 72 . 70 . 72 . 78 . 77 . 78 . 76 . 71 . 72 . 71 . 72 . 70 . 72 . 78 . 77 . 78 . 76 . 70 . 60 . 63 . 63 . 61 . 65 . 66 . 67 . 67 . 67 . 60 . 60 . 63 . 63 . 61 . 65 . 67 . 67 . 67 . 60 . 81 . 81 . 81 . 81 . 78 . 78 . 87 . 87 . 88 . 88 . 77 . 64 . 64 . 64 . 65 . 68 . 68 . 68 . 77 . 64 . 64 . 64 . 64 . 64 . 64 . 68 . 68 . 68 . 77 . 64 . 64 . 64 . 65 . 68 . 68 . 68 . 77 . 64 . 64 . 64 . 65 . 69 . 79 . 79 . 90 . 90 . 90 . 90 . 90 . 90 . 91 . 91 . 91 . 91 . 91 . 91 . 91 . 91					111.)	10 4				
. 74 . 7/ . 7/ . 70 . 79 . 77 . 72 . 49 . 68 . 72 . 76 . 72 . 70 . 78 . 74 . 75 . 73 . 73 . 8/ . 84 . 80 . 83 . 82 . 80 . 78 . 77 . 72 . 93 . 87 . 80 . 87 . 93 . 90 . 93 . 84 . 24 . 93 . 90 . 98 . 93 . 90 . 93 . 84 . 24 . 66/ . 67 . 67 . 67 . 67 . 67 . 62 . 63 . 69 . 67 . 64 . 68 . 68 . 68 . 62 . 63 . 69 . 67 . 64 . 68 . 68 . 68 . 62 . 64 . 68 . 64 . 65 . 70 . 67 . 67 . 62 . 63 . 7/ . 70 . 69 . 67 . 75 . 7/ . 71 . 71 . 67 . 65 . 69 . 78 . 74 . 75 . 8/ . 74 . 75 . 72 . 71 . 82 . 86 . 83 . 83 . 84 . 82 . 91 . 72 . 73 . 81 . 94 . 90 . 90 . 90 . 90 . 91 . 94 . 90 . 90 . 90 . 90 . 91 . 94 . 90 . 90 . 90 . 91 . 94 . 90 . 90 . 90 . 91 . 94 . 90 . 90 . 90 . 91 . 94 . 90 . 90 . 90 . 91 . 94 . 90 . 90 . 90 . 91 . 94 . 90 . 90 . 90 . 94 . 94 . 92 . 95 . 87 . 82 . 84 . 85 . 86 . 85 . 87 . 87 . 10 . 70 . 68 . 10 . 12 . 64 . 63 . 63 . 69 . 64 . 66 . 68 . 68 . 68 . 68 . 68 . 67 . 14 . 70 . 70 . 68 . 10 . 12 . 64 . 63 . 63 . 69 . 64 . 64 . 65 . 88 . 87 . 87 . 10 . 70 . 70 . 70 . 74 . 73 . 73 . 68 . 71 . 73 . 74 . 70 . 70 . 74 . 73 . 73 . 68 . 71 . 73 . 74 . 70 . 70 . 74 . 73 . 73 . 68 . 71 . 73 . 74 . 70 . 70 . 74 . 73 . 73 . 68 . 71 . 74 . 75 . 76 . 77 . 78 . 77 . 78 . 77 . 78 . 87 . 86 . 88 . 83 . 85 . 88 . 92 . 87 . 87 . 86 . 88 . 83 . 85 . 88 . 92 . 87 . 87 . 86 . 88 . 83 . 85 . 88 . 92 . 87 . 87 . 86 . 88 . 83 . 85 . 88 . 92 . 87 . 77 . 87 . 77 . 78 . 76 . 71 . 72 . 71 . 72 . 70 . 72 . 78 . 77 . 78 . 76 . 71 . 72 . 71 . 72 . 70 . 72 . 78 . 77 . 78 . 76 . 70 . 60 . 63 . 63 . 61 . 65 . 66 . 67 . 67 . 67 . 60 . 60 . 63 . 63 . 61 . 65 . 67 . 67 . 67 . 60 . 81 . 81 . 81 . 81 . 78 . 78 . 87 . 87 . 88 . 88 . 77 . 64 . 64 . 64 . 65 . 68 . 68 . 68 . 77 . 64 . 64 . 64 . 64 . 64 . 64 . 68 . 68 . 68 . 77 . 64 . 64 . 64 . 65 . 68 . 68 . 68 . 77 . 64 . 64 . 64 . 65 . 69 . 79 . 79 . 90 . 90 . 90 . 90 . 90 . 90 . 91 . 91 . 91 . 91 . 91 . 91 . 91 . 91	Pressure 1	ratio	0, 0	190						
18					.70	.79.	.77	72	49_	168
9.5 90 90 87 93 90 93 84 84 85 14 16 67 65 64 70 65 64 70 65 64 65 67 67 67 68 68 70 67 62 63 68 67 67 68 68 70 67 62 63 68 68 68 70 67 62 63 68 70 67 67 62 63 68 70 67 67 62 63 68 70 67 67 62 63 68 70 67 67 65 69 78 74 75 75 77 77 75 87 74 75 77 77 77 78 78 78 78		.72	.76	.72	.70	.78	.74	.75		
85 9/ 88 87 90 26 86 24 161 67 65 64 70 65 65 64 68 68 68 68 68 68 68		1								
.61 .67 .65 .64 .70 .65 .65 .64 .63 .64 .63 .67 .67 .62 .63 .67 .67 .64 .68 .68 .70 .67 .62 .63 .67 .67 .62 .63 .67 .67 .67 .62 .63 .67 .67 .67 .62 .63 .67 .67 .67 .67 .62 .63 .67 .67 .67 .67 .67 .65 .69 .78 .74 .75 .81 .74 .75 .172 .21 .67 .65 .69 .78 .74 .75 .81 .74 .75 .172 .21 .82 .86 .83 .83 .84 .82 .81 .79 .78 .91 .41 .70 .70 .90 .86 .80 .90 .90 .81 .86 .68 .69 .64 .64 .65 .63 .68 .64 .64 .65 .63 .68 .64 .64 .65 .63 .68 .64 .64 .65 .63 .68 .64 .64 .65 .63 .68 .64 .64 .65 .63 .68 .64 .64 .65 .63 .68 .64 .64 .65 .63 .68 .64 .64 .65 .63 .68 .64 .64 .65 .63 .68 .64 .64 .65 .63 .68 .64 .64 .65 .63 .68 .64 .64 .65 .63 .68 .64 .64 .65 .63 .68 .64 .64 .65 .68 .68 .64 .64 .65 .68 .68 .64 .64 .65 .68 .68 .64 .64 .65 .68 .68 .64 .64 .65 .68 .68 .64 .64 .65 .68 .68 .64 .64 .65 .68 .68 .64 .64 .65 .68 .68 .64 .64 .65 .68 .68 .68 .69 .69 .89 .89 .89 .83 .85 .81 .81 .73 .73 .64 .71 .74 .70 .70 .70 .70 .70 .70 .70 .70 .70 .70										
.63 .69 .67 .64 .68 .68 .12 .47 .62 .63 .67 .68 .64 .65 .70 .67 .57 .62 .63 .71 .70 .69 .67 .75 .71 .71 .57 .57 .52 .69 .78 .74 .75 .81 .74 .75 .72 .71 .82 .86 .83 .83 .94 .82 .91 .77 .78 .91 .91 .90 .90 .96 .90 .90 .81 .96 .84 .90 .86 .87 .95 .88 .86 .85 .86 .68 .69 .64 .66 .83 .68 .66 .63 .67 .74 .70 .70 .63 .70 .72 .66 .67 .66 .73 .74 .70 .70 .74 .73 .73 .66 .71 .73 .76 .74 .70 .75 .76 .75 .73 .75 .67 .74 .70 .70 .77 .78 .78 .97 .97 .97 .85 .87 .82 .84 .87 .83 .95 .87 .87 .96 .99 .95 .94 .98 .97 .97 .98 .97 .86 .86 .83 .85 .88 .82 .97 .87 .86 .86 .83 .85 .88 .82 .97 .87 .86 .86 .83 .85 .88 .82 .97 .87 .86 .86 .83 .85 .88 .82 .97 .87 .86 .86 .83 .85 .88 .82 .97 .87 .86 .86 .83 .85 .88 .82 .97 .87 .86 .86 .83 .85 .88 .82 .97 .87 .86 .86 .83 .85 .88 .82 .97 .97 .86 .86 .83 .85 .88 .82 .97 .97 .86 .86 .83 .85 .88 .82 .97 .97 .86 .86 .83 .85 .88 .82 .97 .97 .86 .86 .83 .85 .88 .82 .97 .97 .86 .86 .83 .85 .88 .82 .97 .97 .86 .86 .83 .85 .88 .82 .97 .97 .86 .86 .83 .85 .88 .82 .97 .97 .86 .86 .83 .85 .88 .82 .97 .97 .87 .78 .76 .76 .76 .76 .76 .76 .76 .76 .76 .76		1								
.67 .68 .64 .65 .70 .67 .67 .62 .63 71 .70 .69 .67 .75 .71 .21 .67 .65 .69 .78 .74 .75 .81 .74 .75 .72 .73 .82 .86 .83 .83 .84 .82 .91 .79 .78 .91 .91 .90 .90 .96 .90 .90 .91 .96 .84 .90 .86 .87 .95 .88 .86 .85 .86 .68 .69 .64 .66 .88 .68 .68 .66 .63 .69 .74 .70 .70 .70 .70 .71 .73 .73 .66 .71 .73 .76 .74 .70 .70 .74 .73 .73 .66 .71 .73 .76 .74 .70 .75 .75 .76 .75 .73 .75 .85 .87 .82 .84 .87 .87 .82 .87 .87 .96 .99 .95 .94 .98 .97 .97 .92 .97 .86 .86 .83 .85 .88 .22 .97 .94 .94 .73 .72 .70 .7/ .72 .71 .72 .70 .72 .78 .77 .78 .76 .73 .78 .76 .75 .74 .74 .85 .90 .78 .76 .73 .73 .72 .74 .71 .79 .79 .74 .82 .83 .75 .76 .76 .76 .76 .76 .81 .87 .85 .86 .83 .76 .60 .63 .63 .63 .66 .67 .67 .70 .62 .63 .63 .63 .63 .68 .68 .68 .68 .62 .62 .62 .64 .65 .63 .68 .68 .68 .71 .64 .64 .62 .64 .65 .27 .28 .27 .23 .23 .22 .21 .22 .99 .21 .19 .21 .20 .19 .21 .19 .91 .83 .18 .19 .19 .18 .18 .16 .16 .16 .90 .87 .87 .89 .92 .91 .91 .91 .93 .95 .92 .94 .97 .72 .91 .94 .95 .93 .95 .93 .94 .97 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .72 .91 .94 .95 .90 .75 .93 .94 .97 .97 .97 .97 .97 .97 .97 .90 .95 .93 .94 .97 .97 .97 .97 .97 .97 .97 .90 .95 .93 .94 .97 .97 .97 .97 .97 .97 .90 .95 .93 .94 .97 .97 .97 .97 .97 .97 .97 .90 .95 .93 .94 .97 .97 .97 .97 .97 .97 .97 .90 .95 .93 .94 .97 .97 .97 .97 .97 .97 .97 .97 .90 .95 .93 .94 .97 .97 .97 .97 .97 .97 .97 .97 .90 .95 .93 .93 .94 .97 .97 .97 .97 .97 .97 .97 .90 .95 .93 .93 .94 .97 .97 .97 .97 .97 .97 .97 .97										
.71										
.69 .78 .74 .75 .8/ .74 .75 .172 .21/ .82 .86 .93 .83 .94 .82 .91 .79 .78 .91 .41 .40 .90 .90 .90 .90 .91 .81 .86 .84 .90 .86 .87 .95 .88 .84 .85 .86 .68 .69 .64 .66 .83 .63 .64 .64 .65 .74 .70 .70 .68 .70 .72 .64 .67 .75 .76 .73 .74 .70 .70 .74 .73 .73 .73 .66 .71 .73 .74 .70 .70 .74 .73 .73 .73 .66 .71 .73 .76 .74 .70 .75 .76 .75 .75 .72 .75 .85 .87 .82 .84 .87 .83 .25 .87 .87 .102 .46 .94 .92 .95 .95 .92 .94 .95 .96 .99 .95 .94 .98 .97 .97 .98 .97 .86 .86 .83 .85 .88 .82 .97 .94 .94 .73 .72 .70 .71 .72 .71 .72 .70 .72 .74 .78 .77 .78 .76 .78 .76 .78 .76 .76 .76 .76 .76 .79 .94 .82 .93 .75 .76 .76 .76 .76 .76 .76 .81 .87 .80 .81 .73 .72 .74 .71 .78 .79 .84 .85 .86 .83 .76 .80 .80 .80 .80 .81 .87 .85 .86 .83 .76 .80 .80 .80 .80 .81 .87 .85 .86 .83 .70 .80 .80 .80 .80 .81 .87 .85 .86 .83 .70 .80 .80 .80 .80 .81 .87 .80 .81 .73 .72 .74 .71 .78 .79 .94 .82 .93 .75 .76 .76 .76 .76 .76 .76 .68 .68 .68 .68 .68 .62 .62 .63 .63 .61 .65 .70 .68 .68 .68 .68 .62 .62 .64 .61 .62 .63 .68 .68 .68 .68 .71 .64 .64 .62 .64 .65 .27 .28 .27 .23 .23 .22 .23 .24 .26 .19 .21 .19 .21 .20 .19 .21 .19 .81 .81 .18 .19 .19 .10 .18 .16 .16 .16 .90 .87 .87 .90 .92 .93 .92 .91 .91 .92 .93 .95 .93 .94 .96 .94 .97 .92 .91 .91 .92 .93 .95 .93 .94 .96 .94 .97 .92 .91 .94 .95 .90 .95 .92 .94 .97 .92 .91 .94 .95 .90 .95 .92 .94 .97 .92 .91 .94 .95 .90 .95 .92 .94 .97 .92 .91 .94 .95 .90 .95 .92 .94 .97 .92 .91 .94 .95 .90 .95 .92 .94 .97 .92 .91 .94 .95 .90 .95 .92 .94 .97 .92 .91 .94 .95 .90 .95 .92 .94 .97 .92 .91 .94 .95 .90 .95 .92 .94 .97 .92 .91 .94 .95 .90 .95 .92 .94 .97 .92 .91 .94 .95 .90 .95 .92 .94 .97 .92 .91 .94 .95 .90 .95 .92 .94 .97 .92 .91 .91 .92 .90 .95 .92 .94 .97 .92 .91 .91 .92 .90 .95 .92 .94 .97 .92 .91 .91 .92 .90 .95 .92 .94 .97 .92 .91 .91 .92 .90 .95 .92 .94 .97 .92 .91 .91 .92 .90 .95 .92 .94 .97 .92 .91 .91 .92 .90 .95 .92 .94 .94 .97 .92 .91 .91 .92 .90 .95 .92 .94 .94 .97 .92 .91 .91 .92 .90 .95 .92 .94 .94 .97 .92 .91 .91 .92 .90 .95 .92 .93 .92 .93 .92 .93 .93 .93 .90 .92 .93 .92 .93 .92 .93 .93 .93 .90 .92 .93		-			-	-		-	The second of	
. 82 . 86 . 83 . 83 . 84 . 82 . 81 . 19 . 78 . 91 . 91 . 90 . 90 . 90 . 90 . 90 . 91 . 96 . 84 . 90 . 86 . 87 95 . 88 . 86 . 85 . 86 . 68 . 69 . 64 . 66 . 68 . 68 . 68 . 66 . 63 . 68 . 71 . 70 . 70 . 68 . 10 . 72 . 66 . 67 . 66 . 73 . 74 . 70 . 70 . 74 . 73 . 73 . 69 . 71 . 73 . 76 . 74 . 70 . 75 . 76 . 75 . 73 . 15 . 85 . 87 . 82 . 84 . 89 . 83 . 85 . 87 . 87 . 1.02 . 96 . 99 . 95 . 94 . 98 . 97 . 97 . 98 . 97 . 86 . 36 . 83 . 85 . 88 . 82 . 97 . 98 . 97 . 86 . 36 . 83 . 85 . 88 . 82 . 97 . 98 . 97 . 86 . 36 . 83 . 85 . 88 . 82 . 97 . 98 . 97 . 86 . 36 . 83 . 85 . 88 . 92 . 97 . 98 . 97 . 86 . 36 . 83 . 85 . 88 . 92 . 97 . 98 . 97 . 86 . 36 . 83 . 85 . 88 . 92 . 97 . 98 . 97 . 98 . 77 . 78 . 76 . 78 . 78 . 74 . 78 . 74 . 78 . 77 . 78 . 76 . 78 . 78 . 74 . 78 . 78 . 79 . 94 . 82 . 83 . 75 . 76 . 74 . 74 . 98 . 81 . 87 . 85 . 86 . 83 . 76 . 80 . 80 . 83 . 66 . 67 . 67 . 70 . 62 . 63 . 63 . 61 . 65 . 70 . 68 . 68 . 68 . 62 . 62 . 64 . 64 . 65 . 62 . 68 . 68 . 68 . 68 . 62 . 62 . 64 . 64 . 65 . 63 . 68 . 68 . 68 . 68 . 62 . 64 . 64 . 64 . 65 . 27 . 28 . 27 . 23 . 23 . 22 . 23 . 24 . 24 . 19 . 21 . 19 . 21 . 20 . 19 . 21 . 19 . 81 . 79 . 97 . 97 . 90 . 90 . 90 . 90 . 90										
.91										
1.84 .90 .26 .87 .95 .88 .86 .85 .86 .68 .68 .69 .64 .68 .68 .68 .66 .63 .69 .74 .70 .70 .68 .70 .70 .70 .70 .70 .70 .70 .70 .70 .70 .70 .70 .70 .70 .70 .75 .75 .73 .74 .70 .75 .75 .75 .72 .75										
.74 .70 .70 .68 .10 .72 .66 .67 .16 .73 .74 .70 .70 .70 .74 .73 .73 .68 .11 .73 .76 .74 .70 .70 .75 .76 .75 .73 .75 .75 .25 .25 .27 .25 .25 .27 .27 .28 .29 .29 .29 .29 .29 .29 .29 .29 .29 .29		.84	.90	.26	.87_	.95	-88	. 86	.85	
.73 .74 .70 .70 .74 .73 .73 .68 .71 .73 .76 .74 .70 .75 .76 .75 .73 .75 .85 .87 .82 .84 .89 .83 .85 .27 .27 .102 .46 .94 .92 .95 .95 .95 .92 .44 .25 .96 .99 .95 .94 .98 .47 .97 .92 .97 .86 .86 .83 .85 .88 .22 .97 .24 .25 .73 .72 .70 .7/ .72 .71 .72 .70 .72 .78 .77 .78 .76 .79 .78 .78 .74 .74 .74 .74 .85 .90 .78 .76 .81 .81 .78 .75 .75 .78 .78 .80 .81 .73 .72 .74 .71 .72 .79 .94 .82 .83 .75 .76 .76 .76 .76 .76 .90 .81 .87 .85 .86 .83 .75 .76 .80 .80 .83 .66 .67 .67 .70 .62 .63 .63 .61 .65 .70 .68 .68 .62 .62 .64 .64 .64 .62 .64 .68 .68 .68 .62 .74 .64 .64 .64 .65 .65 .27 .28 .27 .23 .23 .22 .23 .24 .25 .19 .21 .19 .21 .20 .19 .21 .19 .21 .18 .18 .19 .19 .18 .18 .16 .16 .16 .90 .87 .87 .90 .90 .90 .90 .90 .90 .90 .90 .90 .91 .93 .90 .92 .93 .92 .91 .91 .91 .95 .93 .95 .93 .94 .96 .94 .95 .95 .95 .90 .55 .53 .57 .39 .34 .37 .45 .45 .45 .52 .47 .48 .53 .32 .27 .21 .22 .24 .31 .36 .52 .41 .43 .51 .21 .22 .24 .31 .36										
.73 .76 .74 .70 .75 .76 .75 .73 .15 .25 .87 .82 .87 .82 .84 .87 .83 .25 .27 .27 .27 .26 .96 .99 .95 .94 .98 .97 .97 .92 .97 .86 .86 .86 .83 .85 .28 .22 .97 .24 .24 .25 .73 .72 .70 .7/ .72 .71 .72 .70 .72 .73 .72 .70 .7/ .72 .71 .72 .70 .72 .73 .77 .78 .76 .78 .78 .78 .78 .78 .78 .78 .78 .78 .78										
1.02		-						_	_	
1,02										
. 96 . 99 . 95 . 94 . 98 . 97 . 97 . 98 . 97 . 86 . 86 . 86 . 83 . 85 . 88 . 82 . 97 . 94 . 24 . 24 . 73 . 72 . 70 . 7/ . 72 . 71 . 72 . 70 . 72 . 78 . 77 . 78 . 76 . 78 . 78 . 74 . 74 . 74 . 75 . 78 . 78 . 78 . 78 . 78 . 78 . 78										
. \$6 . \$6 . \$3 . \$5 . \$8 . \$2 . \$7 . \$2 \ 27 . 73 . 72 . 70 . 7/ . 72 . 7/ . 72 . 70 . 72 . 78 . 76 . 78 . 76 . 78 . 76 . 78 . 76 . 78 . 76 . 74 . 74 . 74 . 74 . 78 . 76 . 78 . 78 . 76 . 78 . 78 . 76 . 78 . 78										
.73 .72 .70 .7/ .72 .71 .72 .70 .72 .78 .77 .78 .76 .73 .78 .76 .74 .74 .83 .90 .78 .76 .81 .81 .78 .75 .75 .78 .78 .90 .81 .73 .72 .74 .71 .72 .79 .94 .82 .83 .75 .76 .76 .76 .76 .76 .90 .81 .87 .85 .86 .83 .76 .80 .80 .83 .66 .67 .67 .70 .62 .63 .63 .61 .65 .70 .68 .68 .68 .62 .62 .64 .64 .65 .27 .28 .27 .23 .23 .22 .23 .24 .25 .19 .21 .19 .21 .20 .19 .21 .19 .81 .18 .18 .19 .19 .18 .18 .16 .16 .16 .90 .87 .87 .98 .87 .85 .83 .82 .84 .90 .91 .87 .90 .90 .86 .89 .88 .87 .92 .93 .90 .92 .93 .92 .91 .91 .25 .93 .95 .93 .94 .96 .94 .95 .95 .25 .90 .95 .92 .94 .97 .92 .91 .94 .95 .60 .55 .53 .57 .39 .34 .87 .45 .47 .52 .47 .48 .53 .32 .27 .27 .37 .41 .54 .43 .43 .53 .22 .21 .26 .31 .36 .52 .41 .43 .51 .21 .22 .24 .31 .36										
78 .77 .78 .76 .78 .76 .78 .76 .74 .74 .74 .83 .90 .78 .76 .81 .81 .78 .75 .75 .75 .75 .79 .94 .82 .83 .75 .76 .76 .76 .76 .76 .90 .81 .87 .85 .86 .83 .76 .80 .80 .83 .66 .67 .67 .70 .62 .63 .63 .61 .65 .70 .68 .68 .68 .62 .62 .64 .64 .62 .63 .63 .61 .65 .27 .28 .27 .23 .23 .22 .23 .24 .25 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .81 .18 .18 .19 .19 .19 .18 .18 .16 .16 .16 .16 .16 .16 .16 .16 .16 .16										
.78 .78 .90 .8 .73 .72 .74 .71 .78										
.78 .78 .90 .81 .73 .72 .74 .71 .74 .79 .94 .82 .83 .75 .76 .76 .76 .76 .80 .81 .87 .85 .86 .83 .76 .80 .80 .83 .66 .67 .67 .70 .62 .63 .63 .61 .65 .70 .68 .68 .68 .62 .62 .64 .64 .62 .64 .65 .27 .28 .27 .23 .23 .22 .23 .24 .25 .19 .21 .19 .21 .20 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .25 .33 .95 .93 .95 .93 .95 .93 .95 .93 .95 .93 .95 .95 .95 .95 .95 .95 .95 .95 .95 .95		.83			1					
8/ 87 .85 .86 .83 .76 .80 .80 .83 .66 .67 .67 .70 .62 .63 .63 .61 .65 .70 .68 .68 .62 .62 .64 .64 .62 .63 .68 .68 .68 .68 .7/ .64 .64 .62 .64 .65 .27 .28 .27 .23 .23 .22 .23 .24 .24 .19 .21 .19 .21 .20 .19 .21 .19 .21 .18 .18 .19 .19 .18 .18 .16 .16 .16 .90 .87 .87 .88 .87 .85 .83 .82 .84 .90 .91 .87 .90 .90 .86 .89 .88 .89 .92 .93 .90 .92 .93 .92 .91 .91 .95 .93 .95 .93 .94 .96 .94 .95 .95 .25 .90 .95 .92 .94 .97 .92 .91 .94 .95 .60 .55 .53 .57 .39 .34 .87 .45 .47 .52 .47 .48 .53 .32 .27 .27 .37 .41 .54 .43 .43 .53 .22 .21 .26 .31 .36 .52 .41 .43 .51 .21 .22 .24 .31 .36		.78				.73	72	74	.71.	.7里
.66 .67 .67 .70 .62 .63 .63 .61 .85 .70 .68 .68 .68 .68 .62 .62 .64 .61 .52 .63 .68 .68 .68 .68 .71 .64 .64 .62 .64 .65 .27 .28 .27 .23 .23 .22 .23 .24 .25 .19 .21 .19 .21 .20 .19 .21 .20 .19 .21 .19 .21 .25 .20 .19 .21 .19 .25 .25 .25 .27 .27 .27 .27 .25 .25 .25 .25 .25 .25 .25 .25 .25 .25										
.70 .68 .68 .68 .62 .62 .64 .61 .52 .63 .68 .68 .68 .71 .64 .64 .62 .64 .65 .27 .28 .27 .23 .22 .23 .24 .25 .19 .21 .19 .21 .20 .19 .21 .25 .25 .25 .25 .27 .27 .28 .28 .29 .29 .29 .29 .29 .29 .29 .29 .29 .29										
.68 .68 .68 .7/ .64 .64 .62 .64 .65 .27 .28 .27 .23 .23 .22 .23 .24 .25 .19 .21 .19 .21 .20 .19 .21 .19 .21 .18 .18 .19 .19 .18 .18 .16 .16 .16 .90 .87 .87 .88 .87 .85 .83 .82 .84 .90 .91 .87 .90 .90 .96 .89 .88 .89 .92 .93 .90 .92 .93 .92 .91 .91 .95 .93 .95 .93 .94 .96 .94 .95 .95 .25 .90 .95 .92 .94 .97 .92 .91 .94 .95 .60 .55 .53 .57 .39 .34 .87 .45 .47 .52 .47 .48 .53 .32 .27 .27 .37 .41 .54 .43 .43 .53 .22 .21 .26 .31 .36 .52 .41 .43 .51 .21 .22 .24 .31 .36										
.27 .28 .27 .23 .23 .22 .23 .24 .25 .19 .21 .19 .21 .19 .21 .20 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .19 .21 .25 .27 .27 .27 .27 .27 .27 .27 .27 .27 .27										
.19 .21 .19 .21 .20 .19 .21 .19 .21 .18 .18 .19 .19 .18 .18 .16 .16 .16 .90 .87 .87 .88 .87 .85 .83 .82 .84 .90 .91 .87 .90 .90 .96 .89 .88 .89 .92 .93 .90 .92 .93 .92 .91 .91 .95 .93 .95 .93 .94 .96 .94 .95 .95 .25 .90 .95 .92 .94 .97 .92 .91 .94 .95 .60 .55 .53 .57 .39 .34 .87 .45 .47 .52 .47 .48 .53 .32 .27 .27 .37 .41 .54 .43 .43 .53 .22 .21 .26 .31 .36 .52 .41 .43 .51 .21 .22 .24 .31 .36										
.18 .18 .19 .19 .18 .18 .16 .16 .16 .16 .16 .16 .16 .16 .16 .16										
.90 .87 .87 .88 .87 .85 .83 .82 .84 .90 .91 .87 .90 .90 .96 .89 .88 .89 .92 .93 .90 .92 .93 .92 .91 .91 .95 .93 .95 .93 .94 .96 .94 .95 .95 .25 .90 .95 .92 .94 .97 .92 .91 .94 .95 .60 .55 .53 .57 .39 .34 .87 .45 .47 .52 .47 .48 .53 .32 .27 .27 .37 .41 .54 .43 .43 .53 .22 .21 .26 .31 .36 .52 .41 .43 .51 .21 .22 .24 .31 .36			/				.,	-dul	,	
.90 .87 .87 .88 .87 .85 .83 .82 .84 .90 .91 .87 .90 .90 .96 .89 .88 .89 .92 .93 .90 .92 .93 .92 .91 .91 .95 .93 .95 .93 .94 .96 .94 .95 .95 .25 .90 .95 .92 .94 .97 .92 .91 .94 .95 .60 .55 .53 .57 .39 .34 .87 .45 .47 .52 .47 .48 .53 .32 .27 .27 .37 .41 .54 .43 .43 .53 .22 .21 .26 .31 .36 .52 .41 .43 .51 .21 .22 .24 .31 .36		. 18	.18	.19	.19	.18	18	.16	.16	.16
.92 .93 .90 .92 .93 .92 .91 .91 .95 .93 .95 .73 .94 .96 .94 .95 .95 .95 .90 .95 .92 .94 .97 .92 .91 .94 .95 .60 .55 .53 .57 .39 .34 .87 .45 .47 .52 .47 .48 .53 .32 .27 .27 .37 .41 .54 .43 .43 .53 .22 .21 .26 .31 .36 .52 .41 .43 .51 .21 .22 .24 .31 .36	_				-					
.93 .95 .73 .94 .96 .94 .95 .95 .75 .90 .95 .92 .94 .97 .92 .91 .94 .95 .60 .55 .53 .57 .39 .34 .87 .45 .47 .52 .47 .48 .53 .32 .27 .27 .37 .41 .54 .43 .43 .53 .22 .21 .26 .31 .36 .52 .41 .43 .51 .21 .22 .24 .31 .36		.90	91	.87	.90	.90	.86	.89	.88	.89
.90 .85 .92 .94 .97 .92 .91 .94 .95 .60 .55 .53 .57 .39 .34 .87 .45 .47 .52 .47 .48 .53 .32 .27 .27 .37 .41 .54 .43 .43 .53 .22 .21 .26 .31 .36 .52 .41 .43 .51 .21 .22 .24 .31 .36		.92								
.60 .55 .53 .57 .39 .34 .87 .45 .47 .52 .47 .48 .53 .32 .27 .27 .37 .41 .54 .43 .53 .22 .21 .26 .31 .36 .52 .41 .43 .51 .21 .22 .24 .31 .36								-		
.52 .47 .48 .53 .32 .27 .27 .37 .41 .54 .43 .43 .53 .22 .21 .26 .31 .36 .52 .41 .43 .51 .21 .22 .24 .31 .36						100000				
.54 .43 .43 .53 .22 .21 .26 .31 .36 .52 .41 .43 .51 .21 .22 .24 .31 .36										
.52 .41 .43 .51 .21 .22 .24 .31 .36										
.56 .51 .50 .56 ,/2 .04 ./3 .18 ,25		,52	.41	.73	27	.21		.27	131	, 06.
.56 .51 .50 .56 .12 .04 .13 .18 .25										
		.56	.51	.50	.56	.12	.04	./3	.18	.25

Table Ib (continued)

14	ble IB (continue	(a)
XP-42 Airplane	Test No Flight No. Rue No.	12-1 12-2 12-2 1 2 3 4 5
Short-nose low- in/et-velocity Cowling	True Airspeed, moh. qc, impact press, in H ₂ 0 Atm. pressire, in. Hg. Ambient Air Temp, F o, density ratio Density Altitude, ft, Rpm Bhp Manifold Press, in Hg	328 329 328 332 331 330 328 327 331 330 355 34.5 33.2 32.7 31.8 34.4 32.8 32.0 31.1 30.1 77/5 16.46 15.80 15.11 14.53 16.46 15.76 15.14 14.54 13.93 5 4 1 -1 -8 7 4 4 1 -5 .640 .616 .595 573 .559 .611 .590 .567 .548 .532 14600 15650 16100 17850 18550 15900 17000 18150 19150 20050 26 80 26 891 863 840 812 891 873 850 821 789 405 39.0 37.7 36.3 35.2 38.9 37.4 36.1 34.8 33.5
	Planton Pless, /// 1/3	Cuff 1, no fan.
		Pressure ratio, Alge
A-TPS A-TPS A-TPS A-TPS A-TPS A-TPS A-TPS A-TPS		75 75 76 75 76 77 76 77 76 76 77 76 77 77 77 77 77 78 86 84 85 85 85 85 85 86 86 91 92 89 90 90 89 92 91 91 92 89 88 88 88 87 87 89 72 71 70 71 71 72 72 72 72 72 72 72 72 73 73 72 72 72 72 73 73 73 72 72 72 72 71 72 73 73
A-ASI A-ASI	A-RPI 2 3 3 8 9 A-RSI 2 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	7.6 75 76 7.5 7.6 7.6 7.6 7.5 7.6 7.6 7.7 7.8 7.6 7.8 7.8 7.6 7.7 7.7 7.8 7.6 7.8 7.6 7.7 7.7 7.7 7.8 7.6 7.8 7.4 7.2 7.2 7.1 7.7 7.8 7.6 7.8 7.4 7.2 7.2 9.7 7.7 7.8 7.6 7.8 7.4 7.2 7.2 7.1 7.2 7.2 7.1 7.2 7.2 7.1 7.2 7.2 7.1 7.2 7.2 7.1 7.2 7.2 7.2 7.3 7.4 7.2 7.3 7.3 7.4 7.3 7.2 7.3 7.2 7.3 7.4 7.2 7.3 7.3
Location of Pressure Tubes in Annulus	A-LPI 2 3 septiment Survey A-LSI 2 3 septiment Survey A-LSI 3	J5 76 76 75 75 76 76 76 75 76 77 J5 75 75 75 75 75 75 76 77 J8 77 76 77 78 77 77 78 77 77 78 77 79 87 87 87 89
O-FSE O-FPE O-SPE O-SPE Shielde	RPI 3) Front Survey 2 3 Survey 2 Survey 2 Survey 2 Survey 2 Survey 3 Survey	. \$\frac{45}{95}\$ \text{95}\$ \text{94}\$ \text{95}\$ \text{95}\$ \text{96}\$ \text{97}\$ \text{1.00}\$ \text{1.00}\$ \text{1.00}\$ \text{1.00}\$ \text{1.00}\$ \text{1.00}\$ \text{1.00}\$ \q
Carburetor Scoop	C-Pl 2 impact tubes	.58 .58 .57 .58 .58 .57 .57 .50 .59 .99 .98 .98 .98 .96 .97 .98 .96 .97 .98 .000 .99 .000 .99 .98 .99 .000 .99 .98 .000 .101 .101 .100 .100 .100 .101 .101
C-P3 0 1 1 1 0 C-S4 0 0 C-P3 0 1 1 1 1 0 C-S4 0 0 C-P3 0 1 1 1 1 0 C-S2 0 0 C-P3 0 1 1 1 0 C-P3 0 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	C-SI 2 3 static tubes 4 5	\$\begin{align*} \$1.00 & .01 & .01 & .02 & .02 & .01 & .01 & .02 & .02 & .01 & .01 & .02 & .02 & .01 & .02 & .02 & .01 & .02 & .02 & .01 & .02 & .02 & .01 & .02 & .02 & .01 & .02 & .02 & .01 & .02 & .02 & .01 & .02 & .02 & .01 & .02
F 4.03 C-SI flush stati	c C-TH Impact press. in contathnoon	.83 .82 .82 .83 .8/ .84 .84 .83 .83

7.	able	I Z	b) (c	con	tina	red.)						2
			3-1					-3				7-2	
	1	2	3	4	5	1	2	3	4	1.	2	3	4
Ind. airspeed, mph.	161	158	150	154	157	138	140	137	137	138	138	137	138
	1	13.3	158	11.6	12.1	9.4	9.6	9.2	6.9	9.3	9.3	9.2	9.3
Pressure altitude	1				19100-		-	-16100-					
range, ft. }			13500					16800				TADD	
Free air temp, F	56	39	29	19	10	90	3.1	13	-1.	2.1.	5.9	13	0
Bhp.	840	880	860	סדר	700	915	890	780	700	910	795	660	580
Manifold pressure	320	39.6	38.4	33.7	30.2	39.7	38.5		30.0	41.7	37.2	39.1	29.1
Rpm		-2	540					a	5,2	1			-
	A. A	-	ch,c	limh		Diss	a my	ch, ch	emh	FIII	4 km	heli	mh
	1101	u //	17,6	,,,,,		_			-	1	11101	100111	,,,~
	-				CUI	7	I,	no	Ta	7			>
Pi	-855	sur	e 1	rati	0, 1	0/9							
,	70	.75	.75	.75	74	.78	.68	.73	.71	.77	.77	72	.70
	.70	.78	.78	.79	.76	.79	.78	.75	.73	.77	.73	.74	.72
	.83	.83	.86	.85	.85	.85	79	.78	.76	.85	.84	.78	.77
	90	.95	95	92	90	97	.87	.85	85	.95	.89	90	.87
	.87	.94	91	.95	90	.95	90	.85	.95	92	.88	.87	.87
	.64	.65	.66	.66	.64	.67	.64	64	.64	.67	.67	.62	.61
	.62	.65	.65	.66	.65	.69	64	66	.66	.69	.69	.69	.63
	.62	.64	.68	.68	.69	.70	67	168	68	.70	.72	.67	.64
	70	.73	.74	.73	70	.78	.74	.7/	65	.74	.72	70	.68
	74	.80	.84	.81	.76	.93	82	.79	.75	84	.82	.76	.76
	1.02	94	1.02	95	99	1.05	95	95	95	1.10	1.10	1.07	1.01
	.88	.96	.96	.97	.93	1.05	99	.95	92	1.04		94	,99
	.64	.65	.64	65	.69	.6:7	65	62	.62	64	.66	.62	.61
	.68	.66	.67	.69	.68	.73	70	.66	64	7/	.69	.68	.63
	69	.7/	.74	.73	.72	74	.69	7/	71	.74	.74	.7/_	70
	.63	68	.67	70	69	.62	65	.65	63	.65	.64	68	.62
	.81	.82	.84	.83	84	.86	84	,89	87	90	.88	.85	81
	97	91	96	.97	94	1.03	99	1.00	98	1.03	1.03	7.03	.97
	1.02	1.06	1.02	1.04	.99	1.08	1.11-	1.09	1.06	1.09	1.08	1.09	1.0
	:89	.86	.84	.85	85	.82	.83	.85	.83	.87	.87	.83	.82
	.70	.72	.72	.72	.71	76	.72	.72	.72	.76	.75	,72	69
	.77	.80	.78	.78	.74	.87	.82	80	.78	87	.82	.80	.77
		.8/	.84	.83	.84	.92	.84	.85	.82	.90	.88	84	.8/
		1.20			1.08					1.23		1.19	1.08
					1.10							1.13	
		96	96	96	93	1.29		1.20			1.00	1.12	
	93	91	.96	.96	93	1.08		99	97	1.02		96	.89
TE TOTAL OF	.88	97	.76	.94	92		1.00.		.94	1.02		98	91
	47	45	47	43	.45	49		47	41	49	48	41	39
	27		.32	30	.31			.32	, ,	37			29
				-30	.29							.29	25
			1.03					97					
					1.02							1.03	
					1.04							1.05	
The state of the s					1.07					1.21	1.13	1.10	1.04
	1.11	1.15	1.12	1.11	1.07	1.27	1.12	1.09	1.05	1.23	1.20	1.10	1.08
	.79	78	.69	.71	.71	.78	57	.55	.55	.53	51	.50	.53
	.75	.72	.64	.66	.65	70	.46	.49	.51	.46	.43	44	.46
	.78	.68	62	.60	.63	65	43	48	48	.50	41	45	47
	.76	.68	.60	60	.63	.65	.43	.46	.50	.48	45	.43	47
						- Age							
	.84	.72	.69	.69	.69	.70	.52	.51.	.51	.50	.49	.50	48

26	Table	I(b) (comt	Invi	ed								
XP-42 Airplane		Flight No.	1		5-1		_		15-			
Short-nose low-	Run Na		/	2	3	4	5	/	2	3	4	5
inlet - velocity	True Airs	need, mon.	330	33/	332	330	332	330	33/	33/	332	330
cowling	ge, impact p	ress, in. HaO	365	35. 5	34.4	33.3	32.3	36.2	35.1	34.3	332	31.6
	Atm. press		17.17									
	o, density	ir Temp, F	646			-9 .584		3	620		-8 581	
	Density !	Altitude, ft.				17250	18350	14500				
	Rpm Bhp		-	000	047		680				430	-
1		Press., in. Hg						914				
		,	-			itt		n				>
			-					Spe				-
			1	Pre	554	re	rat	io,	P/9.	:		
	A-TPI)	1	73	7.2	7 2	.72	7 2	72	.72	כד	71	70
	2	set set	73	.74	.73	.74	73	.74	.74	74	73	73
A-TP5 A-TP4	3}	Top	84	.86	.85	.86	.86	.86	.87	.86	.86	.86
A-TS2 A-TP3	5)	Rake	.93	91	90	91	90	91		.91	90	.89
A-TSI	PI A-TSI)		.69	.69	.69	.68	.68	.68	.69	.69	.68	.68
5	2 3	static tubos	1.69	0 5.	.69	.69	.68	.69		.69	.69	.68
34.4 1	A-RPI	1	.72	.72	.72	.72	.73	.73	.73	.72	71	.72
A-ROY	LP5 2	es es	73	.72	.72	.72	.74	.73	.73	.72	17.	72
A-RSI A-L	3	Right	1.78	.79	.77	.78	.79	.87	.77	.86	.77 .87	.85
10.	5)	Survey	.83	.83	83	.82	.83	.82	81		.81	81
	A-R51)	.0	.68	.68	.68	.68	.68	.68	.69	.69	.68	.68
Location of Pressure	$\begin{pmatrix} 2 \\ 3 \end{pmatrix}$	s fatic	70	.70	.69	.69	.68	70	05.	.69	.68	.69
Tubes in Annulus	A-LPI)	1	.72	.72		.72	.73	.73	.74	.73	.72	.73
	2	*	.74	.75	.75	74	.74	.75	.75	.76	.74	.75
	3	Left	189	88	.83	.84	.83	.84	.83	.83	.81	.88
	5)	Survey	.81	.83	.83	.82	.82	.83	.83	.83	.82	83
	A-451	\$ 50	.69	.71	71.71	70.72	.69	.70	72 72	.71	.70	71
	3)	static tubes	.74	.74	.75	75	75	1	75		.73	.74
Oil Cooler Pressure Tube Loc		[33]	.95	.94	92	94	94	.94	.95	.94	.94	:94
	2	tub	0.0000000000000000000000000000000000000	9 8		.99		1.01				
	-RPL O-FSI	Front	.87	.87	.86	.87	.87	1	.88		.87	89
O-FR3	0-RP3 2	100	.87	88	.8 7	88	.87	.88	.89	.88	.87	.89
	= 0-RPI		.89	.65	.90	.90	.90	.90	.91	.66	.90	90
0-F33 0-SP-	2	Rear	.60			.59	60	.59	.60		.59	.60
shielde impact t	1 3	Survey	5/	57	5 1	57	57	57	50	50	57	57
	C-P1	1	.56	98	.56	99	.98	99	.58	.58	.57	97
Carburetor Scoop	2	impact	1					1.01				.99
	3	tubes						1.02				
C-55	5							1.03				
3 C-P5 0 2 20 C-54	C-5/		.84	.83			.84	.84	.84	.84	.84	.83
\$ C-P3 07 0 C-53	3	static tubes	83		88.	.82	80	.82		.82		
C-P2 0 5 0 C-52 1 5 0	4		79		.80					.79		
	5)											
- 4.03" C-SI	C-TH	in contathrost	20	80	80		.81	8.3	83		.83	84
	press	IN COMA TOPOST		. 0 0								

	7	aul	e I	(b)(c	one	14	de	d)					2
	1		14-	3 4	1	2	3	4	5	1	14	-2	4
-4-0	-		198	1						1			
Ind. airspeed, mph	16/			161					138	-	-	137	
Pressure altitude	4000-	11100	1500	2 1980	2 2400	8400	12300	16100	19700	2 5100	13200	2-1630	1 19550
Av. free air temp. F			14	20400 5		25		6	-10		14100	9	-7
Av. bhp.	875	910	825	705	870	910	900	790	650	945	760	670	580
Av. manifold press.				30./	1								29.0
Rpm		25	5 0-			— d	540	. —			-25	40-	,
	AUT	oric	-	imb			ch, c	IIm	5	FUI	rici	h, C/1	mb
•	<			Cut	f	2,	/	20 1	an				->
	,	Pre	2550	ure	ra	tio,	P/9	c					
	.74	.74	.72	71	.79		.71	.74	.73	.78	15	75	.74
	.80	.76	.78	.72	.81	.81	.80	.76	.70	.83	.75	.75	.76
	1.95	.91	90	88.	.99	.96	.88	.88	.86	.96	.92	.90	.88
	.94	.90	.88	.61	99	.93	.93	.88	.83	.96	.88	.88	.92
	68	.68	.65	.65	.71	71	.69	.69	.70	.72	.72	.67	.70
	.74	.70	.67	.65	.70	.70	.71	.69	.66	.73	.68	.68	.69
	.87	.83	.81	.74		.93	.96	.88	.83	.97	.89	.87	.85
	1.95	1.02	191	.88	1.09		1.07		1.00				105
	.98	.97	91	88	1.07	1.08	1.10	1.02			1.02	1.00	
	.68	.66	.65	.61	.65	.69	10	.69	.65	07.	70	.70	.68
	.74	.74	71	.68	,79	.79	.68	.73	.72	83	.74	.74	.73
	.69	.69	.71	.71	.61	.67	.64	.65	.64	.97	.61	.61	.85
	98	.01	.97	.95		1.04	97		1.02	1.04	.85	1.02	.90
				1.02		1.15		1.06	1.06	1.13	1.06	1.09	1.12
	.88	.87	.85	.83	.86	.88	.82	.84	.83		.83	.83	.88
	.84	.82	.80	.80	.86	83		.81	.83	.88			.82
	114	114	110	1.06	-	124	112	115	115			1.11	1.12
	1.16	1.14	1.13	1.08	1.23	1.31	1.27	1.19	1.17	1.32	1.17	1.15	1.27
	116			1.06					- 1			1.15	
1447	The state of the s	94	.91	90	1.03	1.04	.99	.95	97	1.17	97	.92	.96
	.95			90					99	1.17		.95	
				.30								.29	
	35	33	3 2	.30	36	14	3.2	33	31	31	29	29	31
	109	105	100	96	1.22	1.11	1.00	1.04	97	1.14	1.06	97	93
				1.02									
				1.03									
	1.16	1.14	1.07	1.03	1.27	1.97	1.24	1.16	1.09	1.26	1.11	1.09	1.06
	.87						.67		.58			.51	
	.76	.59	.58	.62	.76	.59	.5 5	.55	.51	.61	41	.44	44
	.74	60	.58	.60	.78	57	.54	48	.51	.61	.41	.44	.44
	.85	.69	.69	.68	.86	,60	.51	.57	.58	.69	.51	,51	.55
	-	-	-			_			-				

							1		Rente .		_
VO 40 1:	Test No - Flight No	1.		8-22		_	١,		8-23		
XP-42 Airplane -	Run No.	1	2	3	4	5	/	2	3	4	
Short-nose low-											
inlet-velocity	True ourspeed mph.	1							328		
cowling	go, impact press, in 140								33.4		
1000 0	Atm. pressure, in. Hg.	17.10							15.91	15.23	14.
With fan, without	Ambient air temp, %	4		-3			9	7	/	-2	-6
CUPS	a, density Fatio	1					1		. 598		
	Density offitude, ft	14 500				18500	14650	_	16550		184
Are recognise	Rpm			680					680		
	Bhp								873		
	Manifold press, in Hg	402							378		
			HIG	n	spee	ed	17.	1917	SP	<i>eeq</i>	7
	†	1									
Cylinder, Point of m	neasurement	Ten	nne	ratu	ire	oF.			,		
	The state of the s	2011	,,,,,,	4/4	7 67		Γ		-		
2 gasker Themoco	suple at rear sp. plug	22-	330	341	247	245	244	340	352	357	2
3									353		
4							100		366 351		
5.		333	307	373	J#/	J#3	344	344	557	03/	5
6		397	337	377	34/	339	342	342	342	347	. 7
7.	F .								404		
8		1							366		
9.									382		
10	_								389		
11.							1		382		
at .									370		
3		3166	375	383	395	390	387	389	395	402	3
4									382		
I - rear & flange a	t base of cylinder	275	279	281	283	285	282	282	287	289	2
2	×	279	281	283	288	288	287	287	291	293	2
2		275	275	277	279	279	278	278	280	282	2
45		268	268	271	271	272	272	272	274	276	2
		266	266	269	268	268	268	268	268	272	2
6		275	277	277	281	279	280	280	280	282	2
7											
8				281					285		
7		1	177.00						289		
	×	1				298	ì		300		
7.				27/					274		
2		1							293		
9									285		
0 - intaka mané	in the second se	-							295		
Q - intake port Aixture at blower r	rim						1		202		
wel on suction sia			62			68		59	59	65	
	" "		2000	65		7/		62	65	65	6
N N DIRECTOR SIN		- DA				65		62	62	65	6
" " pressure "	float chamber	62	62	65	65			- 44		28	
" in carburetar	float chamber	28	62 25	65 22	65			35	28		
" in carburetar ! " in carburetar ! " front spark pl	flaat chamber iug elbow			22	19	16	35	35 65		62	3
" in carburetar " in carburetar freat spark pl.	flaat chamber iug elbow	2.8	25	22	19	16	35	65			_
" in carburetar " in carburetar " freet spark pl. " freer " " ecanded free air	flaat chamber lug elbow ""	28 59	25 56	22 56	19 53	16 50	35 68	65	65	62	_
in corburetor in corburetor in corburetor in corburetor science of the corburetor science of the corpuretor science of the corpuretor science of the corpuretor of the corpure	flaat chamber lug elbow ''''''''''''''''''''''''''''''''''''	2.8 59 22	25 56	22 56 16	19 53 11	16 50 9	35 68 27	65 25	65	16	/
in carburetar in carburetar in carburetar in carburetar science in carburetar science in front of cyl.	flaat chamber lug elbow ''''''''''''''''''''''''''''''''''''	2.8 59 22	25 56 16 25	22 56 16	19 53 11	16 50 9	35 68 27 35	65 25 35	65	62 16 25	1
in carburetar in carburetar in carburetar in carburetar science air in carburetar science at top annular representation of cyl. */	float chamber lug elbow oop ake	28 59 22	25 56 16 25	22 56 16	19 53 11	16 50 9	35 68 27 35	65 25 35	65 19 28	62 16 25	1
in carburetar in carburetar in carburetar in carburetar science of the carburetar science of the carburetar of cyl. In frant of cyl. In earlier from oil of exit from oil oil of exit from oil oil oil oil oil oil	float chamber lug elbow oop ake	28 59 22 28 3/	25 56 16 25 28	22 56 16 22 25	19 53 11 16 22	16 50 9 13 16	35 68 27 35 38	25 25 35 35	65 19 28	62 16 25 28	2 2
in carburetar in carburetar in carburetar in carburetar science of the carburetar science of the carburetar of cyling in front of cyling at exit from oil of the control of cyling in the control of cyling in the c	float chamber lug elbow oop ake	28 59 22 28 3/	25 56 16 25 28 25	22 56 16 22 25 25	19 53 11 16 22 16	16 50 9 13 16	35 68 27 35 38 56	65 25 35 35 35	65 19 28 32	62 16 25 28 50	7 2 2
in corburetor in corburetor in corburetor scar in corburetor scar in corburetor scar in front of cyl. in front of cyl. in exit from oil of cyl. in line out	float chamber flug elbow 0000 ake 1000 cooler	28 59 22 28 31 140	25 56 16 25 28 25 134	22 56 16 22 25 25 25	19 53 11 16 22 16 134	16 50 9 13 16	35 68 27 35 38 56	65 25 35 35 56 131	65 19 28 32 53	62 16 25 28 50 131	1 2 2 4 12
in carburetar in carburetar in carburetar in carburetar scarburetar scarburetar scarburetar scarburetar scarburetar of cyl. in front of cyl. in behind cyl. */ at exit from oil of continuous comparticular scarburetar comparticular scarburetar comparticular scarburetar comparticular scarburetar comparticular scarburetar comparticular scarburetar scarbur	float chamber flug elbow 0000 ake 1000 cooler	28 59 22 28 31 140	25 56 16 25 28 25 134 196	22 56 16 22 25 25 25	19 53 11 16 22 16 134 196	16 50 9 13 16 13 134	35 68 27 35 38 56 131 193	65 25 35 35 56 131	65 19 28 32 53 131 193	62 16 25 28 50 131	1 2 2 4 12 1
in carburetar in carburetar in carburetar in carburetar in carburetar science of the carburetar science of the carburetar of cyl. In front of cyl. In the carburetar comparts of coessory comparts of the carburetary comparts of the ca	float chamber flug elbow 0000 ake 1000 cooler	28 59 22 28 31 140 196	25 56 16 25 28 25 134 196	22 56 16 22 25 25 25 134 196 92	19 53 11 16 22 16 134 196	16 50 9 13 16 13 134 196	35 68 27 35 38 56 131 193 104	65 25 35 35 35 56 131 193	65 19 28 32 53 131 193	62 16 25 28 50 131 196	1 2 2 4 12 11 9
in carburetar in carburetar in carburetar in carburetar in carburetar science air in carburetar science air in carburetar science air in front of cyl. */ " behind cyl. */ " at exit from oil of exit from oil of coessory comparting the coessory coessory comparting the coessory co	float chamber flug elbow oop ake to cooler ment	28 39 22 28 3/ 3/ 140 196 96	25 56 16 25 28 25 134 196 92	22 56 16 22 25 25 25 134 196 92 77	19 53 11 16 22 16 134 196 92	16 50 9 13 16 13 134 196 89 74	35 68 27 35 38 56 131 193 104 86	65 25 35 35 56 131 193 104	65 19 28 32 53 131 193 101	62 16 25 28 50 131 196 101	1 2 2 4 12
in carburetar in carburetar in carburetar in carburetar science of the carburetar science of the carburetar science of the carburetar of cyling in front of cyling in front of cyling in front of cyling in front oil of the carburetary comparts out the carbon of comparts of the carbon of comparts of the carbon of comparts of the carbon of carbon of the carbon of carbon of the carb	float chamber flug elbow oop ake to cooler ment	28 39 22 28 31 140 196 96 77 66	25 56 16 25 28 25 134 196 92 77 66	22 56 16 22 25 25 25 134 196 92 77 66	19 53 11 16 22 16 134 196 92 77 65	16 50 9 13 16 13 134 196 89 74	35 68 27 35 38 56 131 193 104 86 74	65 25 35 35 56 131 193 104 86 77	65 19 28 32 53 131 193 101 86	62 16 25 28 50 131 196 101 86	1 2 2 4 12 19 9

			(00)							
•			9-21				-	9-20	0	
	a	b	-	d	0	a	6	6	d	@
		- Lune		3000						
Ind. airspeed, mph.	156	155	155	155	154	140	139	138	138	130
90	12.1	12.0	12.0	12.0	11.8	9.7	9.6	9.4	9.4	9.4
Pressure altitude?	4700-	9300-	13300-	16900-	19600-		9500-	15.500	17300-	1950
range, ft.S										
Av. free air temp, F	25	21	6	-4	-12	30	19		-3	
Av. bhp.	-	890					890			
Av. manif. press.	40.0		540		39.6	46.0		25		250
Rpm.	7	d .	7 70				0()	~ 0		
	A	uto.	ric	h, cl	imb	,	FUII	11	ch, c	Im
	4	W	th	fan	, u	1				
					,					
Temper		1 - 4	OF							
Terriper	urz	, ,	′				1.0			1
	-									
	1				342					-
					361		358			
	339	352	350	348	346	358	339	326	310	29
		-	0.1	220	225	221	210	200	214	20
					337		3/8			
					361		326			
	1				380		356			
*					375		348			
	1				375	100000000000000000000000000000000000000				
	1				357		337			
					377		362	314	287	27
	350	365	361	363	365	360	348	301	283	26
	260	275	280	280	282	270	276	264	257	25
					277		272			
	254	267	271	271	271	268	268	264	257	25
					264					
					256					
	245	263	27/	273	273	260	262	264	260	25.
	0.00			~~~	070	0.57	2/2	211	212	25
					273					
					288		276			
					269		260			
					280		268			
					273	Town or the same				
	1				280					
	194	191	191		184		178	176	170	16
	135	141	141	135	132	132	138	127	121	113
	48	48	48	48	45	44	47	44	44	4
	51	51	51	48	45	47	47	47	44	4
	51	48	48	45	45	50	47	44	91	38
· ·	45	39	27	14	5	44	41	29	20	11
	66	63	54	45	36	7/	65	54	14	38
	30	26	14	2	-8	33	24	13	4	-4
		-	2.0		,	3-	3.	/~		
	36	33	20	8	9	35	35	23	8	-2
	39	36	27	14	8	7/	55	23	17	0
	48	57	45	39	17	44	38	32	11	-2
	147	147	129		135		138	144	/32	13
	188	194		194			193		187	18
	, 50	81	78	72	66	80	77	68	65	3
	78			100	00	00		-0		
	78				57	59	62	59	56	50
	60	60 54	63	60	57 48	59	50	59	56	
		60	63		48	1.				38

U	TODIE 1	600									
	Test No Flight No.		,	11-1					11-2		
XP-42 Airplane	Run No.	1	2	3	4	5	/	2	3	4	_
Short-nose low-inlet-											
velocity cowling	True airspeed, mph.	330	328	330	330	33/	327	33/	328	330	3.
	ge	35.2	34./	33.2	32.2	3/.3	34.0	33.6	32.0	31.2	3
No fan, no cuffs	Atm. pressure, in. Hg.	17.18	16.70	15.84	15.18	1454	1646	1581	15.17	14.53	13
	Ambient oir temp, F		12		/	-2	2	2		-5	
	o, density ratio			.590					.577		
	Density altitude, ft.	15050				18900	15500			_	2
	Rom	87/		680 834		701	860		2 68 803		-
	Bho Manifold press, in hg			36.4					35./		
	1947111010 goress., we rig.			506					SPE		
		'''	9,,	٥٫٥٥			1	9.,	٠٫٠٠		
		-									_
Cylinder, Point of m	easurement	Ten	per	ratu	re,	of.					
- gasket thermoco	uple at rear sp. plug			336					328		
2	1			327					319		
3		1		340					332		
4				338		342		332	332	132	
				365 3/4		311	362	314	313	312	
5 7				372					369		
8		1		336					328		
7				363					362		
2		1		368			1		364		
		1		376					373		
2		355	357	359	363	368	356	358	358	360	
3		374	376	380	380	385	371	37/	373	375	-
4	-			363					353		
- rear & flange	of base of cylinder	1		278					274		
2				282					278		
3				274					272		
1				272					272		
5	A	1		262 272			1		272		
7		12/2	212	LIL	212	~17	212	~10	412	~12	-
?		270	272	272	2.72	274	270	270	270	270	:
7				282							
2				293					289		
				274			270	270	270	270	2
2				291					287		
9				280							
4	_			285							
- intake port				200					193	191	
lixture at blower rim			a later	140						134	
uel on suction side of		-		65				61		64	
" " pressure " "	" t shows how	1		68		71		64	64	64	
in carburetor floa		65		34		28		27		21	
- front spark plug e	"	74		71			64		61	58	
recorded free air	-	-	30	24			20				_
ir in carburetor scool	00		3/		22			21	18	14	
at top annular rake			3/		22		21		18	14	
		1 20		31			27	27	21	18	1
		155	152	155	152	155	46	146	146	146	1
" in front of cyl. *1		53	.53	44	31	22	24		21	14	1
" in front of cyl. *1 " behind cyl. *1	noler	100	00	, .							1
" in front of cyl. *1 " behind cyl. *1 " at exit from oil co	poler			137		140		137	/37	137	
" in front of cyl. *1" " behind cyl. *1" " at exit from oil co Oil-in line	poler	137	137	137	137	196	199	193	193	196	/
" in front of cyl. *1 " behind cyl. *1 " at exit from oil co Oil-in line Oil out		137 196 95	137 196 92	137 196 92	137 196 89	196	199	/93 83	193	196 79	1
" in front of cyl. *1 " behind cyl. *1 " at exit from oil co Oil-in line Oil out Occessory compartme eft magneto		137 196 95 83	137 196 92 80	137 196 92 80	137 196 89 80	196 86 77	199 86 76	193 83 76	193 83 73	196 79 73	1
" in front of cyl. *1 " behind cyl. *1 " at exit from oil co Oil-in line Oil out Occessory compartme	nt	137 196 95 83 61	137 196 92 80 64	137 196 92	137 196 89 80 72	196 86 77 70	199 86 76	193 83 76 67	193 83 73 67	196 79 73 67	-

	T		10-2	2				10-3	9	
	a	6		d	e	a	Ь	10-0	d	0
- / . / /						100	100	120	140	/25
Ind. airspeed, mph	1				153		9.5	138	9.6	9.3
Pressure altitude]			11.9							
Irange, ft S	5500	10000	14000	17900	20500	4500	9200	11100-	15400	20700
Av. Free our temp, of	32	18	2	-3	-9	41	18	10	3	-10
Av. bhp			880					830		
Av. manifold press.	39.6		510		297	42.1		38.6 5 4 5		204
Rpm										
	AU	tor	ich,			Fu.			lim	5
	-		- N	o ta	n, n	OCU	115			
Temp	erat	ure	, 0	_						
	348	353	359	353	355	362	363	337	3/7	289
	.338	346	351	346				326		
	357	361	368		200	367	371	359	352	330
		270		355		339	352		335	309
	32.3	378	336	389	385	376	378		380	307
	372	382	391		4001		374		386	367
	333	338		348	348	33/	339		345	
	357	0		383		361	359		378	360
	357			385		350	359	359	359	
		357 351		380			354	324		285
-	368	378	380		387	003		330		276
	365	374	372	368		367		333	311	278
	282	286	293	288		264	279	272	267	254
	278	288	29/	291	288	2 ==	270	274	217	200
	269	276	278	285	2.78			274		263
	254				263			256		248
	267	276	282	282	282	248	270	274		269
	2/2	07.	2 00	200	200	240		775		236
		276			278			272		265
	276		295					283		
	261	269			274			254		
					285			261		
					280			263	254	
	193	188	285		286	193	277	176	174	252
	149	143	137	134	131	136		133	118	109
	56	56	56	56	56	60	60	60	60	60
	62	59	56	56		63	63	60	60.	
	348	56	53	50	50	69 54	63	54	54	54
	7/	62	53	50	47	81	66	54	51	35
	36	23	8	4	-2	44	22	14	8	-4
	34	25	12	6	0	+4	23	16	10	-3
	38	28	12	6	0	47	23	19	13	0
	155	34	152	152	155	51	35	23	19	136
	47	28	22	10	3	54	44	32	26	4
	152	143	152		134	145	154	136	142	130
	193	196	196	193	190	172	189	189	186	183
	80	74	68	62	59	81	72	66	60	56
	71	56	56	50	62	78	76	69	54	63
	62	56	53	47	44	69	63	57	54	44
							-	,		, ,

, -	2,000	-									
	Test No Flight No.		/	2-1					12-2	,	
XP42 Airplane	Run No.	1	2	3	4	5	/	2	3	4	5
Short-nose Low-Inlet-											
	True Airspeed, mph.	200	920	220	772	321	230	728	327	231	230
velocity cowling											
	ge, impact press., in. H.O	33.3							32.0		
	Atm. Pressure, in. Hg.	1									
	Ambient Air Temp., F	5		/			7	4	4	/	-5
	o, density ratio	.640	.616	.595	.573	.559	.611	.590	.567	.548	532
	Density Altitude, ft.	14500	15650	16700	17850	18550	15900	17000	18150	19150	20050
	Rpm	-				-26	80-				
	Bhp	925	891	863	840	812	891	873	850	821	789
	Manifold Press., in Hg										
	774777574 77600.,77479	1.010	07.0	0		ih s					
		1		CIII	cf	1,	h	n Fo	200		
				UUI	, _	-)	''	0 / 0	,,		
the same of the sa									_		
Cylinder, Point of me	asurement				Ten	per	ratu	re,	F		
		220	222			-			349	752	341
1. Gasket thermocouple	an rear spark plug										
2									351		
.3		346							362		
4									353		
A.		372	372	376			369		377		
6		337	337		341	343	331	336	340	347	351
2		376	374	376	376	376	367	371	373	380	384
7									351		
9									388		
AQ:		-							384		
		1							390		
11.											
12									379		
/3									396		
14	· · · · · · · · · · · · · · · · · · ·								371		
1 - Rear & flange at	base of cylinder	280	278	280	282	282	272	277	281	283	280
2											
3		276	274	274	278	278	270	275	277	281	283
# Committee of the comm		274	274	274	276	278	270	272	275	279	279
4		267	263	263	265	265	261	261	264	266	268
		278	276	278	278	280	272	275	277	281	28
7											
8		278	276	278	278	278	270	272	275	279	279
9									290		
10									296		
//									275		
12									294		
/3									281		
14									286		
10 - Intake port									199		
Mixture at blower rim		144	141	138	138	135	141	138	135	138	135
Fuel on suction side of	pump	67	70	67	70	70	79	79	79	79	79
" " pressure " "	"	70	70		73	70		82		79	82
" in carburetor float	t chamber	67	67		67	67	73		73	76	73
11 - Front spark plug e		36		26					32		
II - Rear " "	"	80	77	73	73			76			73
Recorded free air		23		19	17	10		22		19	/3
	222			20							
Air in carbunstor sci		33							25		
" at top annular rake				20		13	1		32		
" in front of cyl. I			10000	26		17			29		
		150		150					159		
" behind cyl. /				21	23	17	45	35	38	35	29
" behind cyl. I " at exit from oil coo	ler										
occurred chi.	ler								132		
" at exit from oil coo	ler	132	138	132	135	132	132	135		135	132
" at exit from oil coo Oil-in line Oil out		132	138	132	135	132	132	135	132	135	132
" at exit from oil coo Oil-in line Oil out Accessory compartmen		132 191 92	138 197 89	132 191 86	135 194 86	132 1 94 83	132 191 92	135 191 92	132 191 92	135 194 92	132 194 89
" at exit from oil coo Oil-in line Oil out Accessory compartment Left magneto		132 191 92 86	138 197 89 83	132 191 86 83	135 194 86 80	132 1 94 83 77	132 191 92 85	135 191 92 85	132 191 92 82	135 194 92 82	132 194 89 79
" at exit from oil coo Oil-in line Oil out Accessory compartmen	nt.	132 191 92 86	138 197 89 83 75	132 191 86 83	135 194 86	132 1 94 83	132 191 92 85 81	135 191 92 85 77	132 191 92 82	135 199 92 82 73	132 194 89

	To	610	II.	- C	OM	tine	100	1							0.
	T		13-1	,	1	-	Te ye	13-3	3		T		13-2	3	
	a	6	0	d	e	0			d	ē.	0				P
Ind. airspeed, mph.				154					137				136		
Pressure altitude				11:7			9.4			9.2	1	9.2			9.4
range, ft	2700	8600	13700	17700	20600	2900	8400	13800	17400	20780	4700	10100	14800	10000	20600
Av. free air temp, of	56	42	29	17	7	47	20	21	12	-3	36	22	22	10	-2
Av. bhp	850	890	870	750	680	870	910	890	770	690	960	920	760	640	570
Av. manifold press.	1			. 33.0	29.3	39.7	3.4.7	38.1			1	41.7	363	31.6	28.6
Rpm.		-a.	540		0					2 5	10-				
	AU.	to 1	rich,	clin	de	AU	to r	ich,	clim	b	FO	IT	ich,	clim	b
						Cu	eff	1,	no	Far	2				
	7	am	Der	ati	ira	0	F				-		***********		
						1		201	200	258	241	750	214	241	202
						1									282
				376											
	-			385	1000										342
															301
															324
	1														350
															344
	-														33/
															307
															284
•	265	286	288	288	288	254	272	283	29/	289	260	280	269	262	258
	1			293							-		-		
				281											256
															245
															262
															246
															273
															275
	252	272	279	281	279	239	263	278	283	283	245	262	262	260	256
															258
															252
				293											
				151											
				75									56		
	75	75	75	75	75	38	58	58	38	55	59	36	56	56	5.6
	65	56	43	33	23	64	33	30	30	33	47	34	34	28	12
	97	94		75		95	74	74	74	67	80	74	74	68	56
	59	47	34	24	16	51	23	27	17	2		27	27	16	4
		49		26	16	52		36	20	4		28	31	19	9
	59	<i>49 56</i>	36 43	26 36	16	52	30	36	23	20	53	38	31	19	9
The second second second				169					176				155		
			65		49	58		42		39	50	44	53	28	12
	154			132					132				137		
	181			194		170	191	191		191			185		
	94	91	85 85	81	75	86	77	70	70	70	74	68	68	63	65
	72	69	65	62	64	64	58	55	55	49	62	53	53	50	47
	75	75	69	65	59		64		38	5.8		56	56	53	50
										La constitution of the con		- Service			

	34	Table II (con	TIT	404								
1	XP-42 Airplane	Test No Flight No.		1.	5-1				15	5-2		
1	,,, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	Run No.	/	2	_	4	5	1	2	3	4	5
1	Short-nose - low-											
	inlet-velocity	True airspeed, mph.	330	33/	332	330	332	330	331	33/	332	330
	cowling.	ge, impact press, in H20				33.3						
	commy.	Atm. Pressure, in. Hg	177			15.18						
		Ambient air temp.	","			-9	44 00 0	3		-5		
-			in			.594						1000
		o, density ratio				17250						10000
-		Density altitude, ft	-	15200	10000		684		15450	ran	1 1100	1000
Ì		Rpm	OIA	087	OL'E	340			224	872	830	811
		Bhp					-					
1		Manifold press., in. Ha	40.5	20.7		36.3				310	20.7	JT.7
						H19				6an		
					6	uff	^	,	10	an		
1												
	Cylinder, Point of measureme	ent			Te.	mpe	rati	re,	F			
1			3/7	310	7/7	325	327	221	221	330	338	326
+	1 - Gasket thermocouple at	rear spark plug				325						
	2					330						
	3					336						
	4		325			332						
	5		23/			372						
	6					334						
	7					366						
	8					349						
+	9					383						
	10					379						- 2 - 2 - 2 - 1
-	//					376						6 6
-	/2					370						
1	/3					376						
-	14					347						
- 1	1 Repr & flange at base	e of cylinder				272						
	2					278						
	3					270						
	4					270						
-	5					259						22000
	6		274	210	272	272	273	275	275	278	280	279
-	7											
1	8		272	268	270	272	273	275	273	275	278	279
	9		285	283	285	287	288	290	290	290	296	295
	10		289	287	289	296	295	296	293	298	300	299
	//					268						
	/2.					289						
	/3					276						
	14					278						
1	10 - Intake port					191						
	Mixture at blower rim		1000			132		V-0		137		
	Feel on suction side of pur	סת				59			66	66	_	72
	" " pressure " " "					59		66	69	72		75
	" in carburetor float chair	mber		56			59		66	66		66
	11 Front spark plug elbow			25		19	16		30	24		18
	11 Rear " " "		68		65		59		69	69	66	62
-	Recorded free oir		19	16	13	9	7	21	18	14	11	8
	Air in carpuretor scoop		25	22	16	13	9	27	24	18	14	14
	" at top annular rake		22	19	16	13	9	27	24	18	14	11
	" in front of cyl. /		25	25	19	16	13		27	21	18	14
	" behind cyl. 1		143			144				145		-
	" of exit of oil cooler		25	22	16	16	9		30		2/	14
+						141	The second second			134		1
	Oil-in line		*	193			194			194		
	Oil out		-									
	Accessory compartment		86		77	78	14		87		85	80
	Left magneto			74	7/		-11		80	78	75	75
	Pilots cockpit			65		68	66	7/	71	71	69	69
1	Recording-instrument comp	artment	56	56	56	56	50	62	62	56	56	36
-												

Table II (con	clu	dec	1)									3.
			1-3	,			4-1	,			14-		
28 112	9	6	C	d	9	6	C	d	•	0	6	C	d
Ind. airspeed, mph	163	163	161	161	142	140	140	139	138	138	139	137	137
, ,					9.9	9.7	97	9.5	93	94	9.5	9.2	92
Pressure altitude	1400-	3200 4	4400-1	9450	/300 3300	6500	H500	15500	19400	4700	1200	15800	20400
Av. free air temp., of	0.000	30		-5		28		6	-10			10	-8
Av. bho					870								
Av. manifold press.	399	40.7	36.0	303	39.7	398	39.1	33.8	297	43.0	400	33.3	288
Rpm	-	25	50-	-				2	5 4	0 -			
	Qui	m ri	chic	limh	AU	ito i	rich	chr	b	Ful	1 ric	5 -16	200
	71.00	0 //	6//2								,,,,,	7,000	
					uff	2		70	fai				-
11-2-21-		Terr	per	rati	ure	0	=						
					349						37/		28
					356								
(367	369	367	361	3/5	377			352		308	34/	3/7
		378	385	378	373	382					397	367	34:
	339				336								
					367								
					34/								
			376							100		367	
					354								
					354							328	
			387			388	/	401			403		
					367								
					249	280						270	257
		289		285	247	272			W		296		257
					245								
	1				230								
	244	276	280	278	238	27/							
	220	0/0		70.	-							250	
					230 247							279	
					247								
					238								
	251	278	285	282	247	278	287	291	291	272	285	268	257
					249								
					251								
					139					154		178	
			67				62			60		60	
	70		67	67			62			63	60	60	57
	67	45	29	13	59	43	35	24	8	60	41	26	10
	101	83	70	61	93	84	74	71	59	94	82	66	54
	6/	38	2/	3	50	32	21	10	-4	41	24	12	-3
	67	45	29	9	59	37	27	14	4	44	32		0
	70	45	29 39	19	59	37 43	27	14 27	18	54	32	16	3 16
			156						169	166	166	151	
	73	51	58	/.3	62	56	34	24	11	63	51	41	19
		156		138			136		142				130
	186		145	195					196	187		187	
	95	83	79	76	87-	78	14	68	62	82	79	72	57
	79	73	67	58	71	65	62	56	59	66	60		69
	83	76		58	14	68		59	53	72	63		51

TABLE III

AVERAGE PRESSURE RECOVERIES ON FRONT OF ENGINE

	-	1		
		Average eng	ine front	pressure, p/qc
Installation		Full power climb		High speed
		. 140 mph	155 mph	
Fan only	12,000 f	0,98	0,95	0,84
	19,000 f	.92	.92	
Cuffs l	12,000 f	.86	.81	.80
	19,000 f	.78	.80	
Cuffs 2	12,000 f	.84	.82	.77
	19,000 f	.82	.78	
No fan nor cuffs	12,000 f	.74	.75	.76
	19,000 f	.72	.73	
Fan and cuffs l (reference 3)	12,000 f	1.02	.95	.87
	19,000 f	.97	,92	

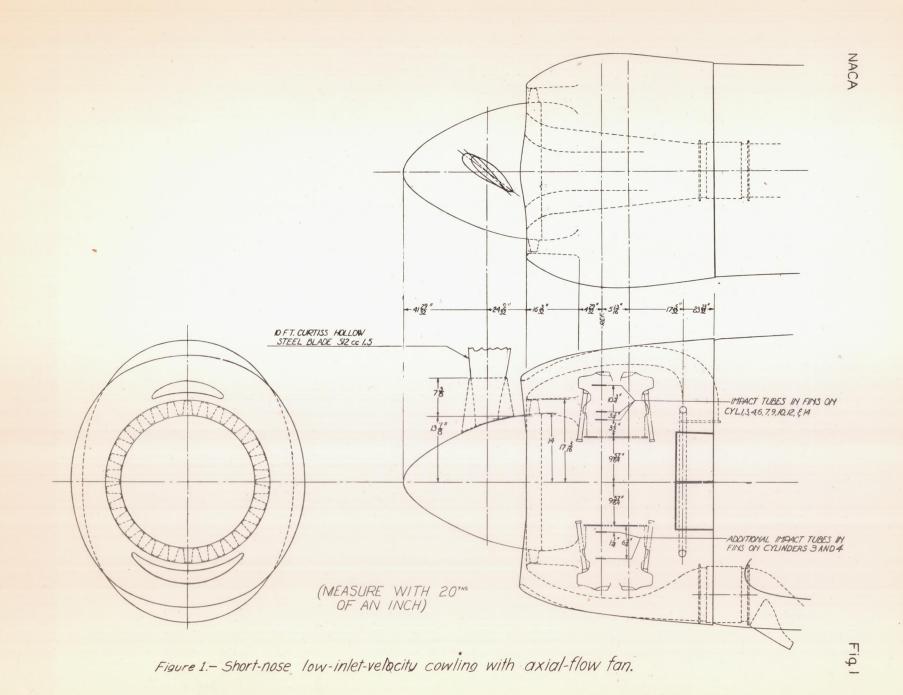




Figure 2.- Side view of XP-42 airplane with short-nose low-inlet-velocity cowling and cuff 1 (test 12).

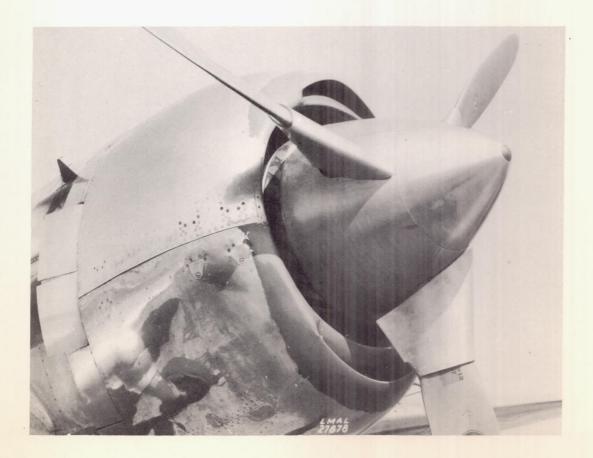
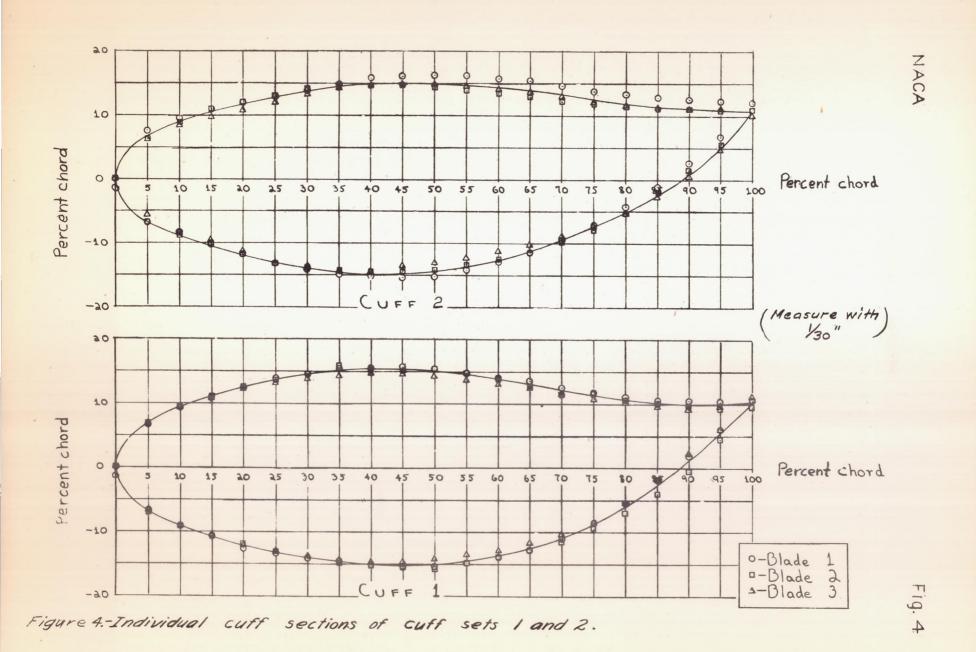


Figure 3.- Close-up of cowling with cuff 2, without fan (test 15).



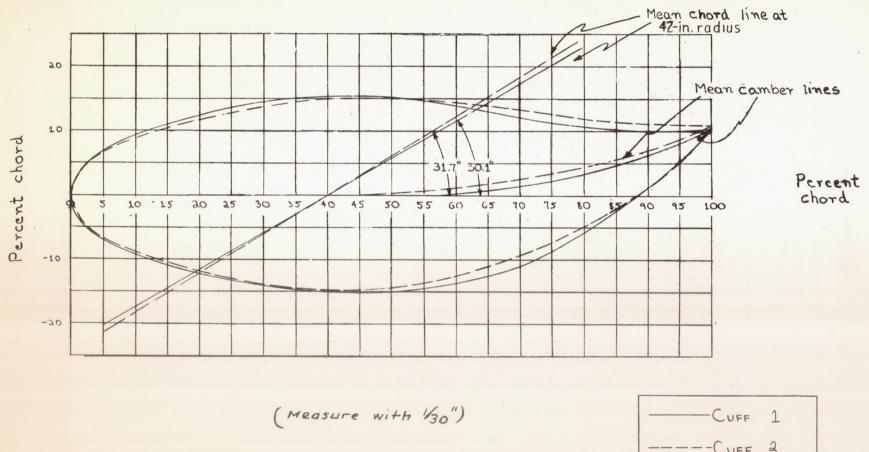


Figure 5- Comparison of average cutt sections of cutts | and 2.

Figure 6 .- Time history of climbs. Test 9 (fan only).

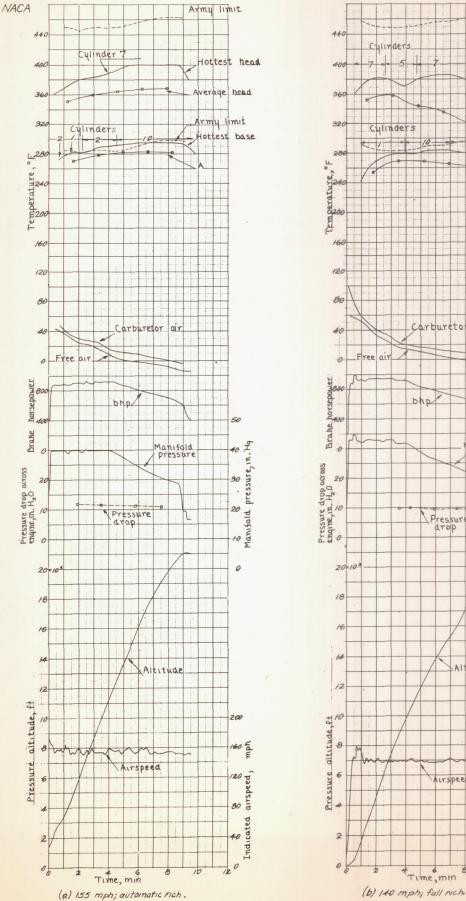
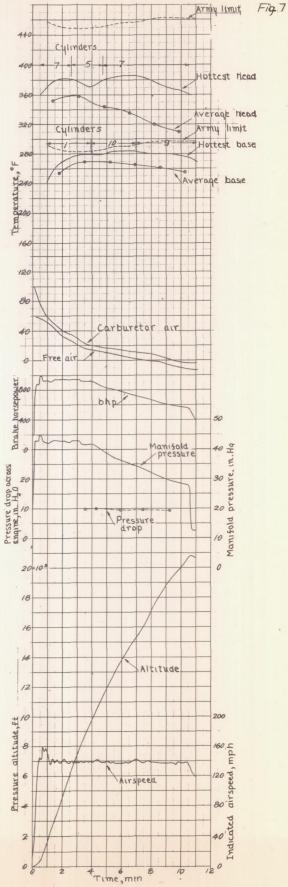
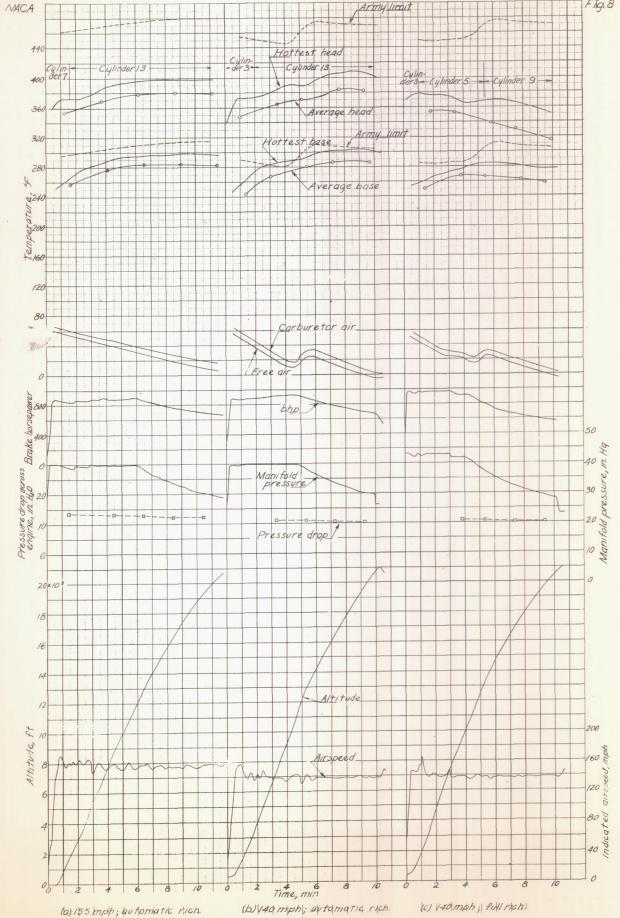
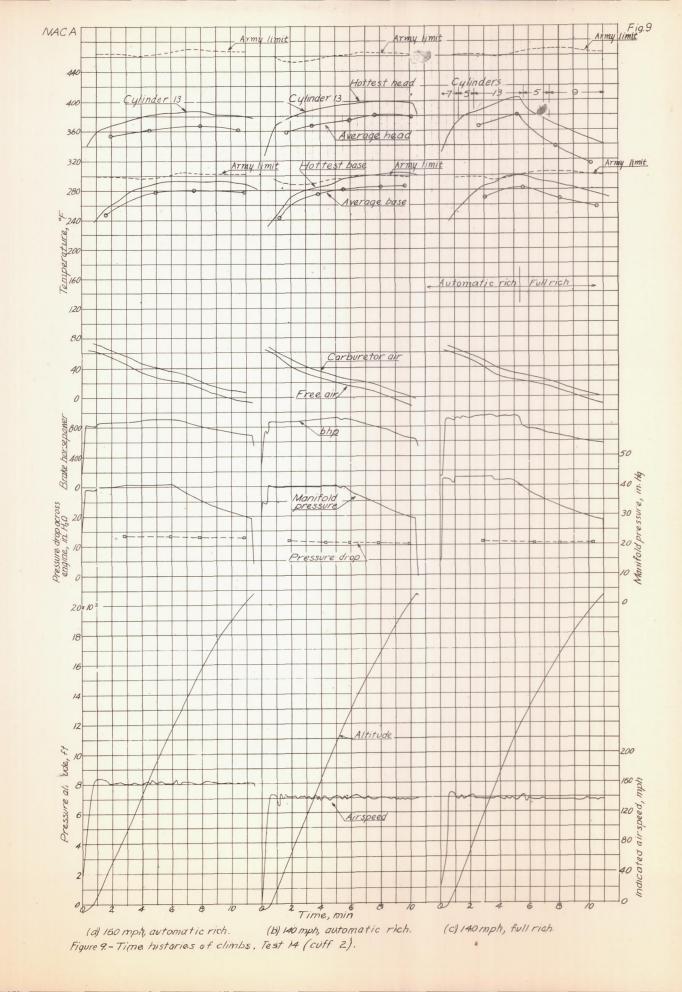


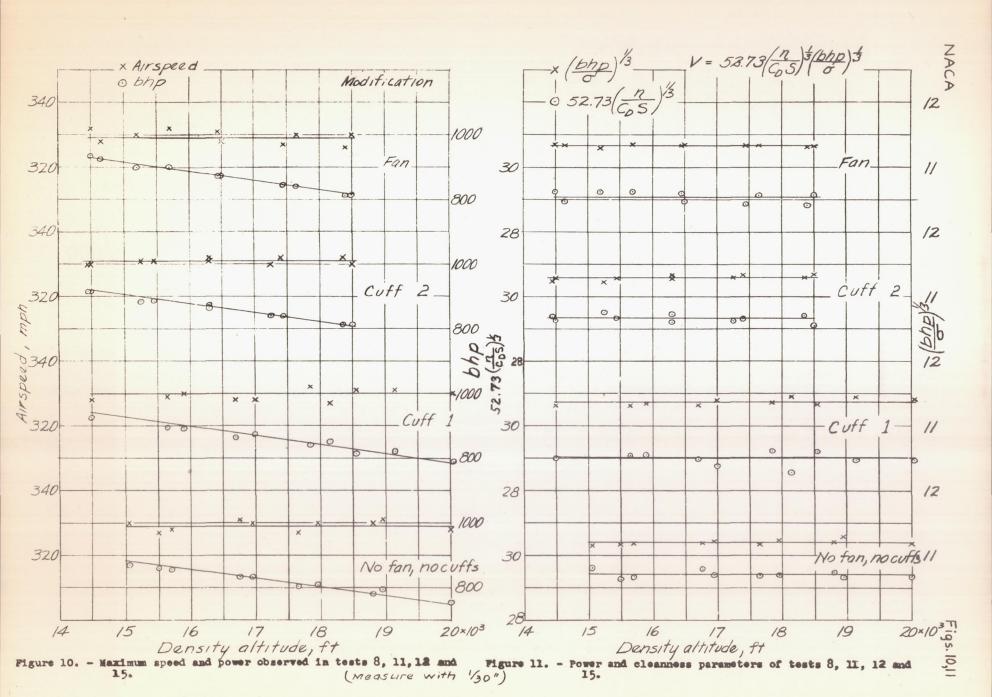
Figure 7.- Time histories of climbs. Test 10 (no fon or cuffs).





1a). 155 mph; automatic rich. Figure 8. Time histories of climbs. Test 13. (cuff 1).





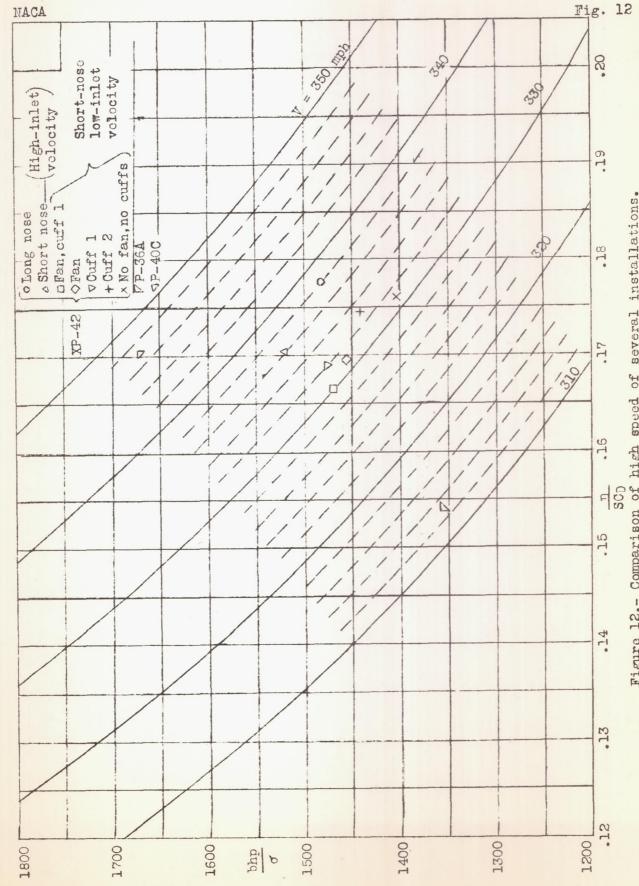


Figure 12.- Comparison of high speed of several installations.

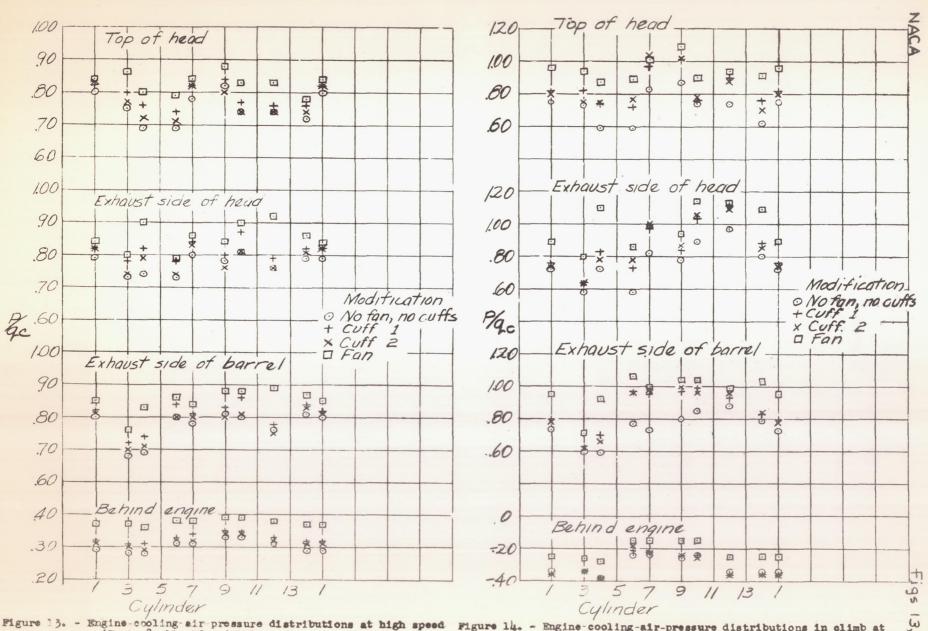
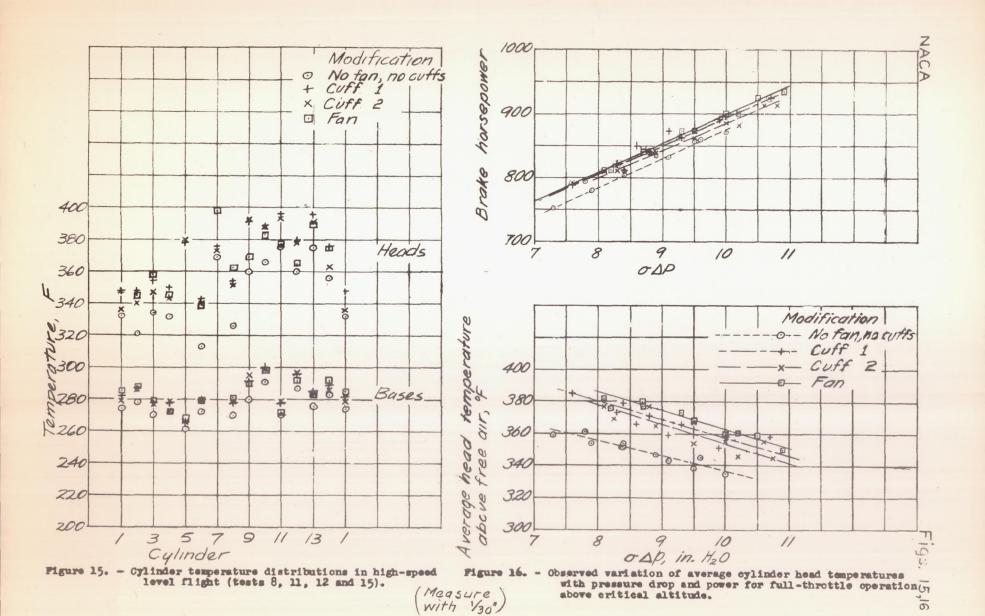


Figure 13. - Engine-cooling-air-pressure distributions at high speed Figure 14. - Engine-cooling-air-pressure distributions in climb at ("ents 8, 11, 12 and 15). (Measure With 1/30")

[Measure With 1/30"]

[Measure With 1/30"]



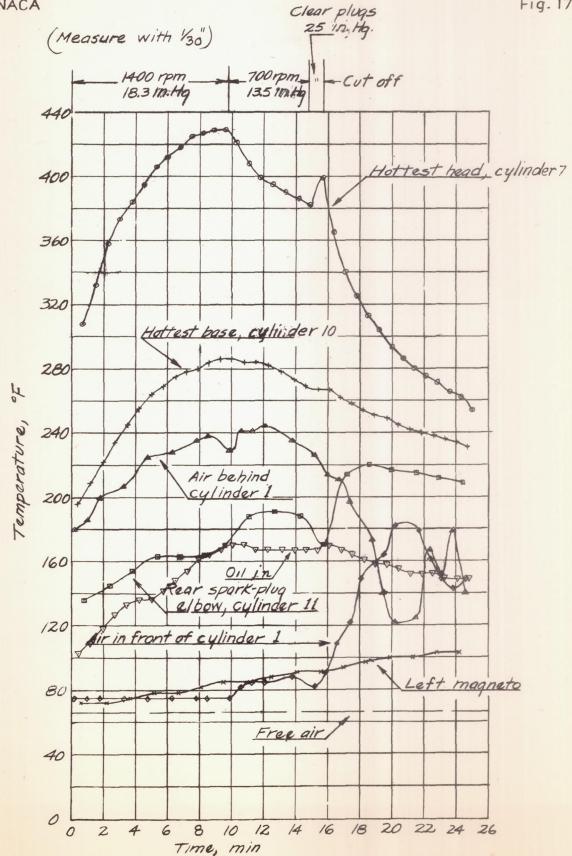


Figure 17-Temperatures in ground run without fan or cuffs.

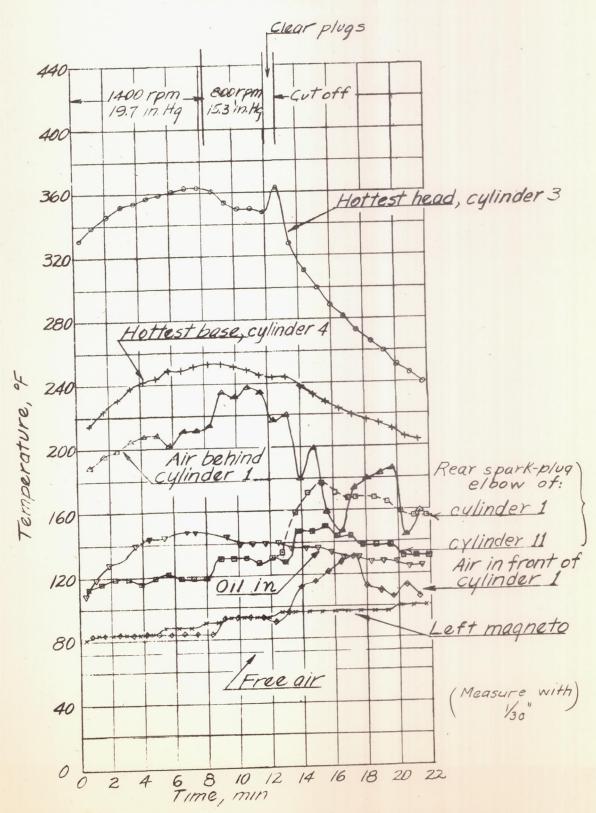


Figure 18. Temperatures in ground run with cuff 1.

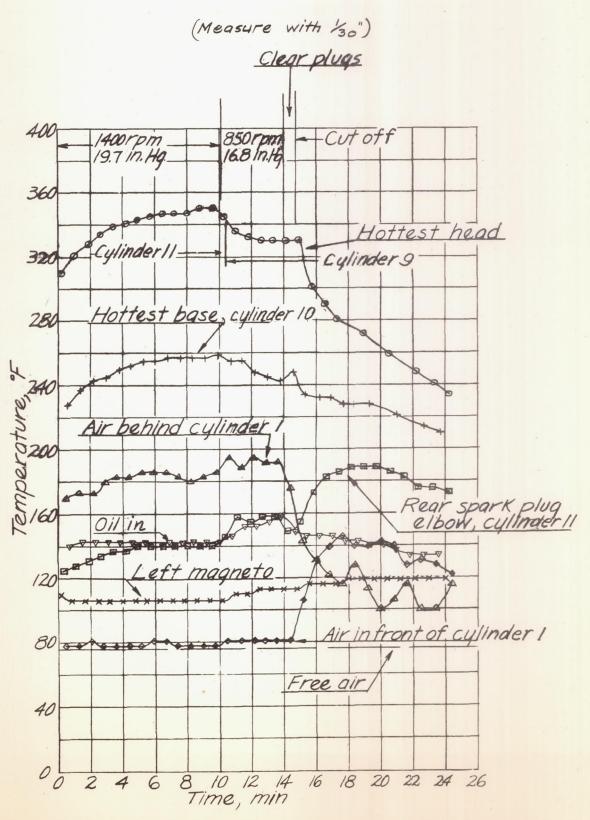


Figure 19. Temperatures in ground run with cuff 2.